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DESCRIPTION AND  
FINAL REPORT

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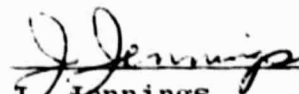
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Date: September 8, 1977

IUE/IRA SYSTEM DESCRIPTION  
AND FINAL REPORT

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## ABSTRACT

The information contained in this document consists of inputs from several IUE/IRA project personnel.

The major sections describe the basic system, its operation, options and parameters.

The Appendix summarizes the test data obtained from the Flight Unit during its ATP.

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## 1.0 INTRODUCTION

The IUE/IRA System is a rate sensor system designed to meet the requirements of the NASA International Ultraviolet Explorer spacecraft mission. The system consists of two units, a Sensor Unit and an Electronic Control Unit. The Sensor Unit (SU) contains six rate sensor modules. The Electronic Control Unit contains the rate sensor support electronics and the command/control circuitry. Together they form an Inertial Reference Assembly (IRA) which will provide spacecraft rate (or delta position) information for use in the stabilization and control system.

The IUE/IRA is designed to meet objectives of a three year mission with an ultimate goal of five years. Highly reliable electronics and sufficient functional redundancy is provided in order to meet these goals.

The succeeding paragraphs will describe the system in terms of functional description, operation, redundancy performance, mechanical configuration, weight, power, mechanical interface and electrical interface.

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## 2.0 SYSTEM BLOCK DIAGRAM

Two block diagrams were generated in order to fully describe the IRA system. They are shown in figures 2-1 and 2-2. Figure 2-1 illustrates a top level breakout of the units with minimal definition. The system is divided into two packages, one containing only the rate sensors and one containing the supporting electronics.

The rate sensor package, called the Sensor Unit, consists of six 64 PM-RIG gyro units each having a pulse rebalance loop mechanization integral within the overall gyro dimensions. The rebalance loop electronics are mounted integral with the gyro in order to provide a rate sensor module which is temperature stabilized and functionally interchangeable with other units. The gyro itself is a fluid floated unit containing a hydrodynamic spin motor bearing.

The supporting electronics package, called the Electronic Control Unit contains a redundant set of command/control electronics, known as the "common electronics" and the required circuits to fully support the rate sensors. This unit contains twelve (12) electronic circuit cards. They are grouped as follows:





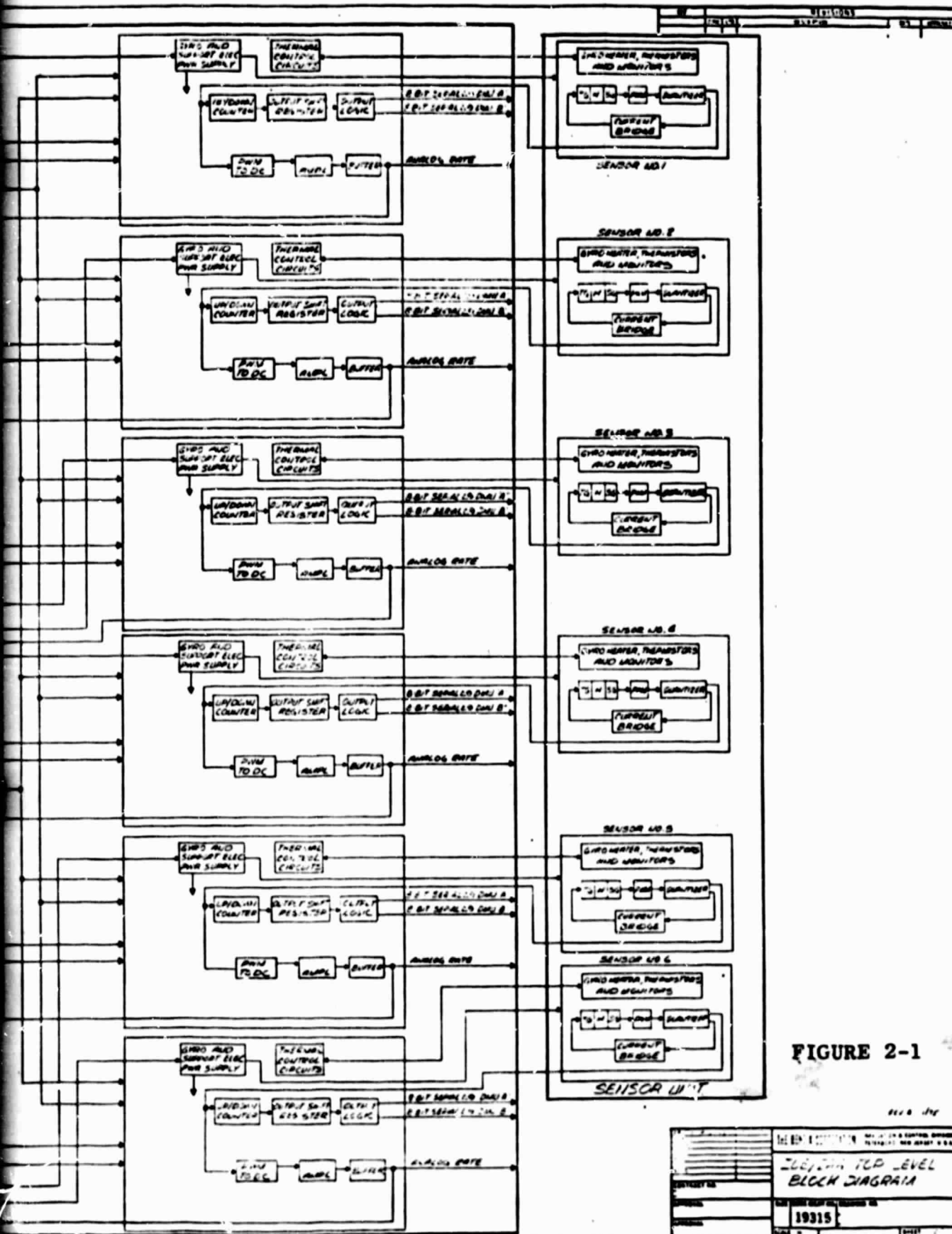
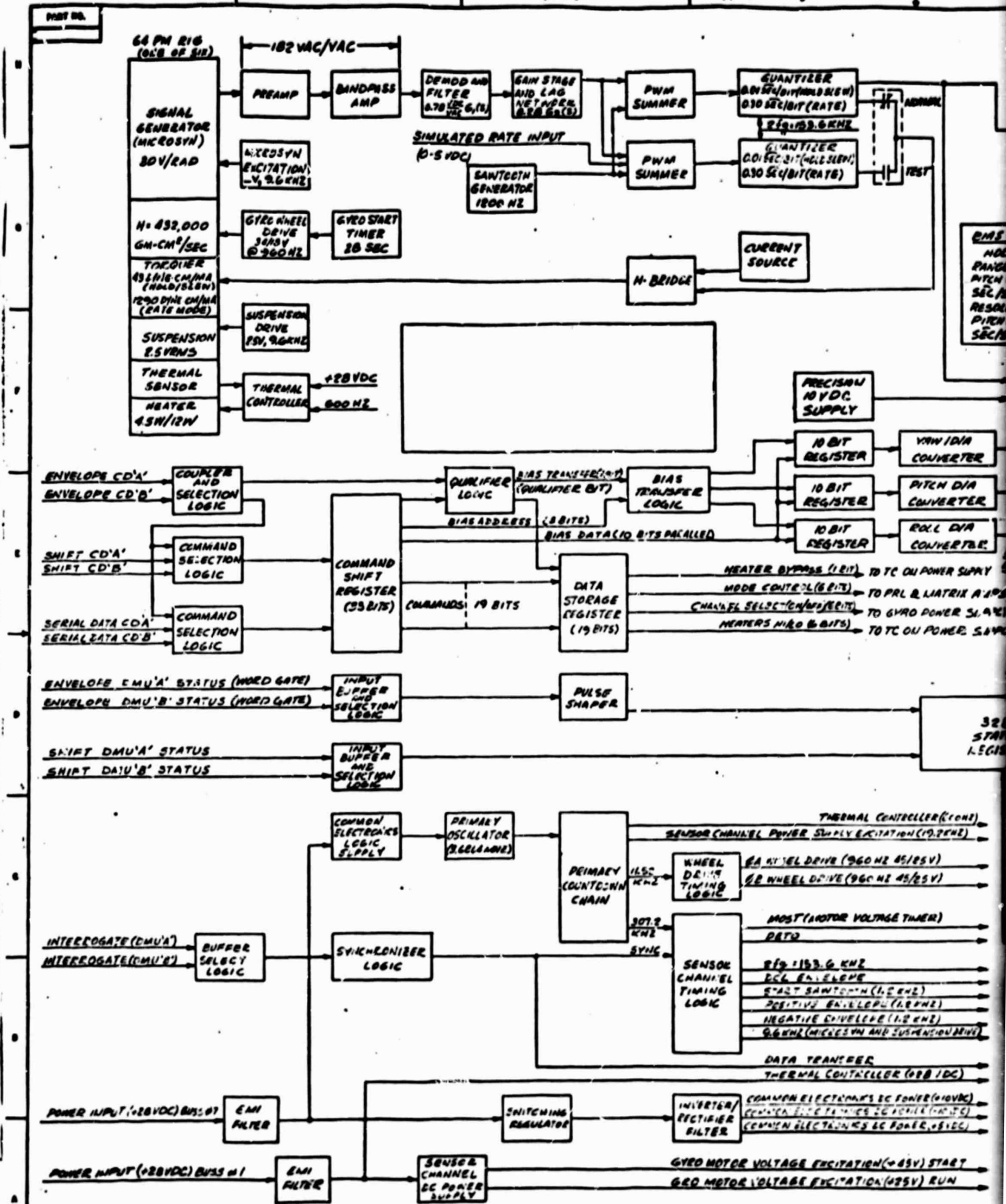


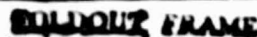
FIGURE 2-1

EXPLODED FRAME



☐ DO NOT MARK PART NO.  
☐ MARK PART NO. AS SPECIFIED

~~SOLD OUT PRICING~~



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2.0 (continued)

- o Common Electronics - 2 cards; one complete set per card; contains the common electronics power supply, system reset logic, main oscillator and countdown chain, command decoder interface, command generation, storage registers, status register interface, status register, interrogate conditioning logic and the pitch, yaw and roll body rate telemetry buffer amplifiers.
- o Gyro Channel Power Supply and Temperature Controller - 3 cards; each card supports two rate sensors; contains the temperature controller hybrid circuit and drive stage, heater mode switching relays, logic for heater switching, transformer, inverters and conditioning for gyro power generation and channel select logic.
- o Support Electronics - 3 cards; each card supports two rate sensors; contains the two phase gyro wheel drive circuitry, microsyn excitation and monitor, spin motor sync detector, gyro temperature monitor conditioning amplifier, suspension drive and monitor.



- o Control Electronics - 3 cards; each card supports two rate sensors; contains the  $\Delta\theta$  output register, 16 bit up-down counter, output logic, logic circuitry for the data, envelope, shift and interrogate, precision 10VDC supply for PWM to DC conversion, timing logic and analog rate telemetry output.
- o Matrix Amplifiers - one card; supports both common electronics cards; contains the digital to analog converter for bias compensation generation, bias compensation amplifiers, body rate matrix amplifiers and gain switching mechanization for the matrix amplifiers.

The common electronics each address all six rate sensors. The ability is provided to switch from one set of common electronics to the other and to command any combination of rate sensors into operation. This is more fully described in the system operation section.

Figure 2-2 illustrates the IRA system on a single axis basis, that is, one set of common electronics, one rate sensor and one set of rate sensor supporting electronics. Major electrical functions are described in the following subsections.

## 2.1 Digital Data Output ( $\Delta\theta$ )

The gyro senses vehicle rate which is converted through hybrid circuitry to PWM format and then quantized. The up/down counter accumulates the quantized pulses which represent the net torque required to rebalance the gyro float (a measure of the net displacement). This information is shifted to the output register and gated to the appropriate Data Multiplex Unit upon command. The output is 8 bit serial data representing  $\Delta\theta$  with two 8 bit segments necessary to obtain one full data word. The up-down counter is sixteen bits in length and operates in 2's complement form. Thus it counts up to  $\pm 16,384$  bits. There is no saturation detection logic required and the counter will increment in the positive direction through saturation to the next binary number (a negative number in 2's complement). The spacecraft computer algorithm will operate on the data and determine the change in inertial position (or rate) by insuring that it sample the data at a rate faster than the time required to overflow the up-down counter for that particular mode. The spacecraft sampling rate is defined as 2-160 times per second. The fastest rate the IRA may be sampled is once every duty cycle or 1200 times per second. The two 8 bit output registers are connected in a non-destruct read fashion, that is, the data is shifted out and recycled back into the register prior to the

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next interrogate. This allows continuous sampling of the same register contents without update. The sampling rate is not restricted by the IRA and any rate sensor may be sampled in any sequence.

In addition, no data is lost in transmission during the sampling time. This is accomplished as follows: The fundamental frequency  $f_s$  is 1200 Hz. The quantizing frequency,  $2f_q$  is 153.6KHz. Therefore, there are 128 pulses or time slots within each  $1/1200$  sec. interval (64 positive and 64 negative). Eight pulses of the 64 are reserved for "housekeeping" functions resulting in a duty cycle of  $56/64$  or 87.5% for data. It is during the remaining 12.5% of the time that the data in the up-down counter is interrogated (shifted to the output registers).

Saturation of the quantized PWM operation occurs at  $\pm 672$  arc seconds per second in the hold/slew mode and  $\pm 5.6^\circ$  per second in the rate mode. Quantization level is 0.01 arc sec per bit in the hold (slew mode and 0.30 arc sec per bit in the rate mode. The analog outputs (body matrix amplifiers and analog rate) are scaled such that saturation occurs at lower levels.



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## 2.2 Body Rate Matrix Outputs, Rate Output

Two forms of analog rate are available at the IRA interface, spacecraft body rates and individual gyro rates.

The spacecraft body rates are determined by summing the outputs of rate sensors 1, 3 and 5 with appropriate magnitude and sign into a set of amplifiers called the matrix amplifiers. There is one such circuit for each of pitch, yaw and roll. A second set of body rates is generated from rate sensors 2, 4 and 6 when common electronics B is used. The ranges and scaling of these outputs are shown in Table 2-1.

Axis	RATE MODE		HOLD/SLEW MODE	
	Body Rates (deg/sec)	Scale Factor vdc/deg/sec	Body Rates (arc sec/sec)	Scale Factor vdc/arc sec/sec
Pitch	$\pm 5$	1.0	$\pm 600$	0.050
Yaw	$\pm 5$	1.0	$\pm 600$	0.050
Roll	$\pm 60$	1.0	$\pm 7200$	0.050

TABLE 2-1 MATRIX PARAMETERS

Saturation occurs at  $\pm 5$ VDC which corresponds to the maximum rate in the rate mode but only  $\pm 100$  arc seconds per second in the hold/slew mode. A better resolution is required for these outputs in this particular mode.

A check on the rate levels for either rate or hold/slew mode may be made by monitoring the individual gyro rate outputs. These outputs are available on telemetry and are scaled such that  $\pm 5$  degrees per second and  $\pm 600$  arc seconds per second equals  $2.5\text{VDC} \pm 2.5\text{VDC}$  (that is 0-5VDC centered at 2.5).

### 2.3 Bias Compensation Generation

A circuit function is provided to bias the outputs of the matrix amplifiers. Ten bits of the input command word are used in 2's complement form to generate a maximum bias of  $\pm 25.6$  degrees per hour to pitch and yaw and  $\pm 307.2$  degrees per hour to roll in the hold/slew mode. Resolution is 0.05 arc second per bit, pitch and yaw, and 0.60 arc second per bit in roll. The bias compensation feature is not eliminated in the rate mode but does change by the matrix scaling change. Range and resolution for pitch and yaw in the rate mode are 0.213 degrees per second and 1.5 arc seconds, respectively. Range and resolution for roll are 2.56 degrees per second and 18 arc seconds, respectively.

### 2.4 Pulse Rebalance Loop

The pulse rebalance loop of each of the six rate sensors consists of six hybrid modules; a preamp and bandpass filter, demodulator and notch filter, gain change and buffer

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amplifier, sawtooth generator and dual quantizer, torquer current source, and torquer H-bridge. These six hybrids are physically mounted to the signal generator end of the gyro and consequently become temperature stabilized with the gyro. The 2nd half of the dual quantizer is used for the simulated torquing test condition. In that mode the feedback to the torquer H-bridge is switched from the normal output quantizer to the test quantizer. An analog input is commanded to the test PWM and the gyro is rebalanced (the signal sum at the test PWM is zero). The normal PWM and quantizer will then read the commanded rate by outputting  $\Delta\theta$  information through the normal output chain.

The frequency of operation of the quantizer (1200Hz) is high enough when compared to the bandwidth of the loop (approx. 7.5 Hz in the hold/slew mode) that the pulse rebalance loop can be considered essentially linear. The nominal closed loop transfer functions for the two modes of operation are shown in Table 2-2. Detailed analysis of the bandwidth and stability criteria is given in MT 37,308.

MODE TEMP	RATE	HOLD/SLEW
80 °F	$\frac{(\frac{S}{6.28} + 1)}{(\frac{S}{8.27})^2 + \frac{2(.69)S}{8.27} + 1} \frac{S}{1010} + 1$	
135 °F	$\frac{(\frac{S}{6.28} + 1)}{\frac{S}{6.33} + 1 (\frac{S}{625})^2 + \frac{2(.21)S}{625} + 1}$	$\frac{(\frac{S}{6.28} + 1)}{(\frac{S}{8.23} + 1)(\frac{S}{26.2} + 1)(\frac{S}{640} + 1)}$

TABLE 2-2 NOMINAL CLOSED LOOP TRANSFER FUNCTIONS FOR THE PULSE REBALANCE LOOP

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The remaining information on Figure 2-2 describes functionally the system power and timing generation and the status register monitor (see Table 2-3 for status register definition). Details are given on the gyro parameters and pulse rebalance characteristics. Additional scaling, weighting, signal ranges and limits will be added to the block diagram during future updates.

### 3.0 SYSTEM OPERATION

#### 3.1 Launch and Transfer Orbit

During launch and transfer orbit the IRA common electronics and rate sensors will be off. Power (limited) will be applied to all six rate sensor heaters. This power is applied by commanding six of the eight spacecraft +28V buss lines to the IRA to be energized. By closing those relays, power will be applied directly to the rate sensor thermal controllers. The thermal controllers will be preset to a latched state that will energize a 4.5 watt heater winding on each gyro. The gyro heaters front end electronics and EMI filters will draw a total of 30.0 watts in this mode (assuming all gyros are below the steady state 135°F).

TABLE 2-3  
STATUS REGISTER SIGNALS

<u>BIT NO.</u>	<u>FUNCTION</u>	<u>STATE</u>
1	Not Used	---
2	Not Used	---
3	Not Used	---
4	Not Used	---
5	Control Bit	"1"=On
6	Rate Cold Mode	"1" =Off
7	Gyro No. 6 Sync/No Sync	"1"=Sync
8	Gyro No. 5 Sync/No Sync	"1"=Sync
9	Gyro No. 4 Sync/No Sync	"1"=Sync
10	Gyro No. 3 Sync/No Sync	"1"=Sync
11	Gyro No. 2 Sync/No Sync	"1"=Sync
12	Gyro No. 1 Sync/No Sync	"1"=Sync
13	Common "A" On/Off	"1"=On
14	Common "B" On/Off	"1"=On
15	Gyro No. 1 Heater Hi/Lo	"1"= Lo
16	Gyro No. 2 Heater Hi/Lo	"1"= Lo
17	Gyro No. 3 Heater Hi/Lo	"1"= Lo
18	Gyro No. 4 Heater Hi/Lo	"1"= Lo
19	Gyro No. 5 Heater Hi/Lo	"1"= Lo
20	Gyro No. 6 Heater Hi/Lo	"1"= Lo
21	Gyro Channel No. 1 On/Off	"1"=On
22	Gyro Channel No. 2 On/Off	"1"=On
23	Gyro Channel No. 3 On/Off	"1"=On
24	Gyro Channel No. 4 On/Off	"1"=On
25	Gyro Channel No. 5 On/Off	"1"=On
26	Gyro Channel No. 6 On/Off	"1"=On

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TABLE 2-3 STATUS REGISTER SIGNALS (continued)

<u>BIT NO.</u>	<u>FUNCTION</u>	<u>STATE</u>
27	Gyro No. 1 Mode, Hold-Slew/Rate	"1"=Hold-Slew
28	Gyro No. 2 Mode, Hold-Slew/Rate	"1"=Hold-Slew
29	Gyro No. 3 Mode, Hold-Slew/Rate	"1"=Hold-Slew
30	Gyro No. 4 Mode, Hold-Slew/Rate	"1"=Hold-Slew
31	Gyro No. 5 Mode, Hold-Slew/Rate	"1"=Hold-Slew
32	Gyro No. 6 Mode, Hold-Slew/Rate	"1"=Hold-Slew

TOTAL = 32

TOTAL USED = 28

SPARES = 4

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As Figure 3-1 shows, the common electronics in the IRA (both sets) draw power from separate busses (No. 7 and No. 8). This method of implementation eliminates the use of impulse commands, allows power to be supplied to gyro heaters without energizing the common electronics and adds to the overall system reliability by reducing the possibility of a multiple failure caused by a short on a power line.

It should be noted that during this mode the thermal controllers are not operating in their normal Pulse Width Modulated state but are operating in an open loop hard-over arrangement. This implementation minimizes power losses and maximizes heat delivered to the gyros.



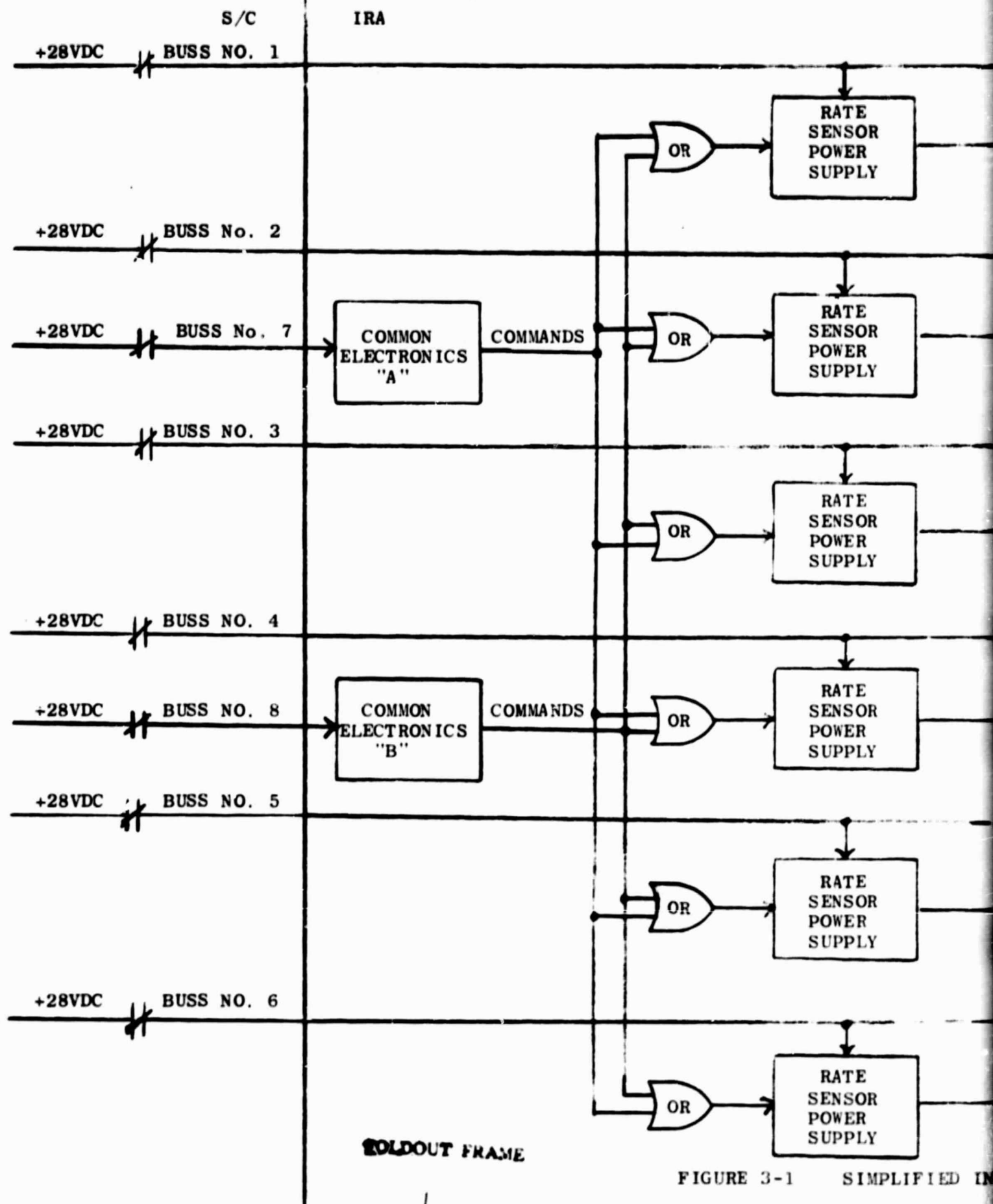
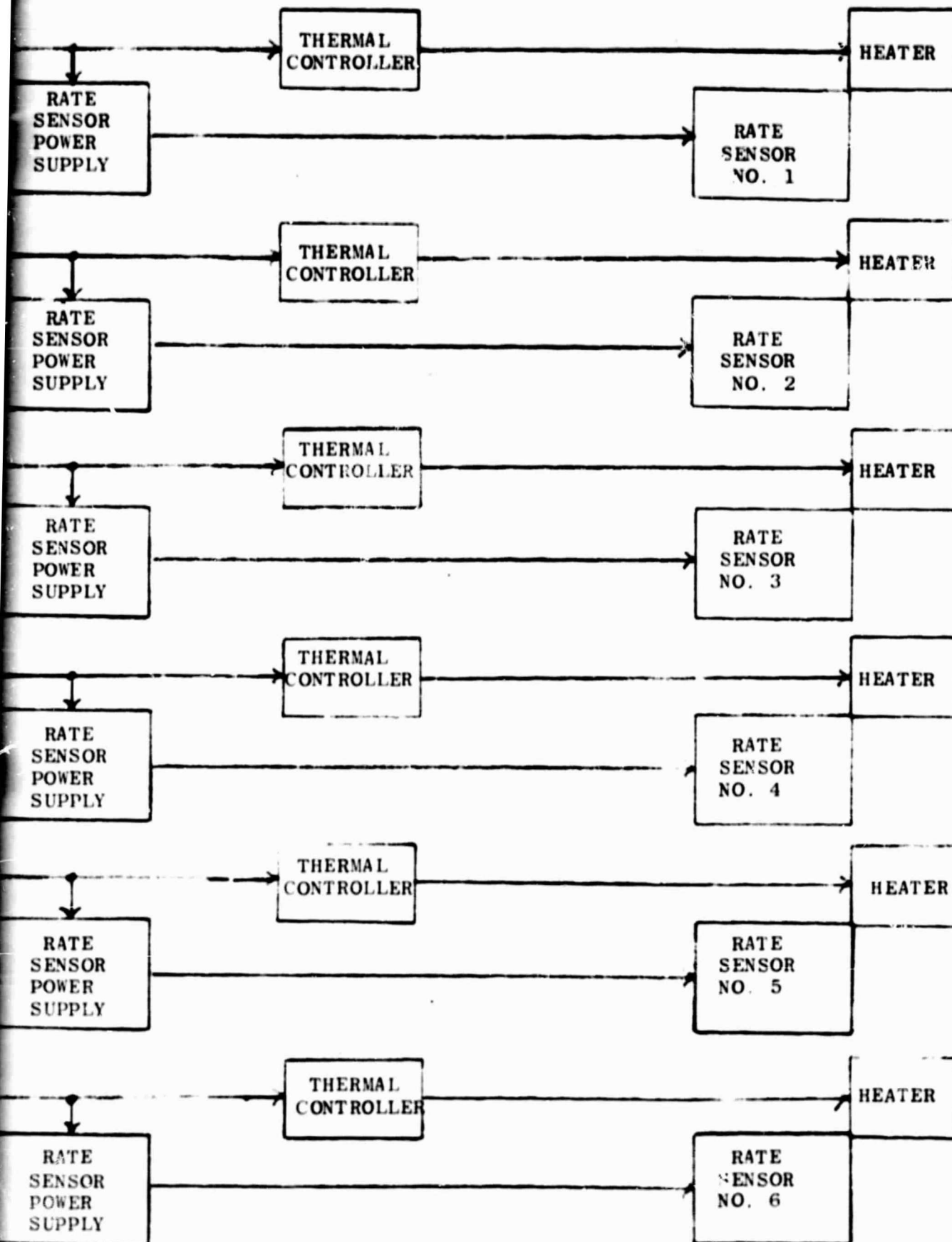


FIGURE 3-1 SIMPLIFIED IN



### 3.2 Initialization On-Orbit

With

30 watts of power available for heating, the steady state non-operating temperature is in the neighborhood of 70°F. Therefore, when the system is fully energized the heaters will still be in a hard-over condition.

To energize the system either Buss No. 7 or Buss No. 8 must be activated by the spacecraft. Closing either of these relays will energize the common electronics power supply (Buss No. 7 for Common "A", Buss No. 8 for Common "B").

The "come up" state of the common electronics is as follows:

- o All gyro channels come up off
- o Gains are set to the rate mode condition
- o Gyro heaters come up in the 4.5 watt state  
(should be in this state from transfer orbit)
  
- o Status register will indicate present states
- o Bias compensation will be reset to zero bias,  
all axes

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- o Gyro sync detectors are reset to "no sync"
- o Matrix amplifier gains are set to rate mode  
(condition is - if any rate sensor is in the hold/slew  
mode then the matrix gain is set to hold/slew).

In general, the input holding registers for the command word are held low during power turn-on. Commands may now be issued to the IRA through the Command Decoder Interface. All IRA commands are issued in this manner. No impulse commands are used.

An option is also provided at this time to initiate the high heater state to one or more gyros. If power is available, the 12 watt heater state can be used to stabilize the IRA in a shorter period of time.

The rate sensors may now be energized. Each rate sensor is energized separately through the channel select command bits. The initial starting power for each rate sensor

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is shown in Figure 3-3. The voltage applied to the gyro wheel during start is 34 VRMS at 960 Hz. To limit power drawn from the spacecraft the rate sensors should be energized sequentially. Power drops off significantly as the gyro wheel reaches sync but still remains higher than the run power until the excitation voltage is reduced to 18VRMS. This occurs 28 seconds after the on command is issued.

The expected sequence is to energize all six rate sensors sequentially, remaining in the rate mode of operation. The spacecraft will then be despun. If necessary, three rate sensors may then be commanded off to conserve power until a sun fixed attitude is obtained. When full power is available the three rate sensors will be energized again and the hold/slew mode commanded. Normal spacecraft experiments will commence when the IRA has been stabilized at 135°F.

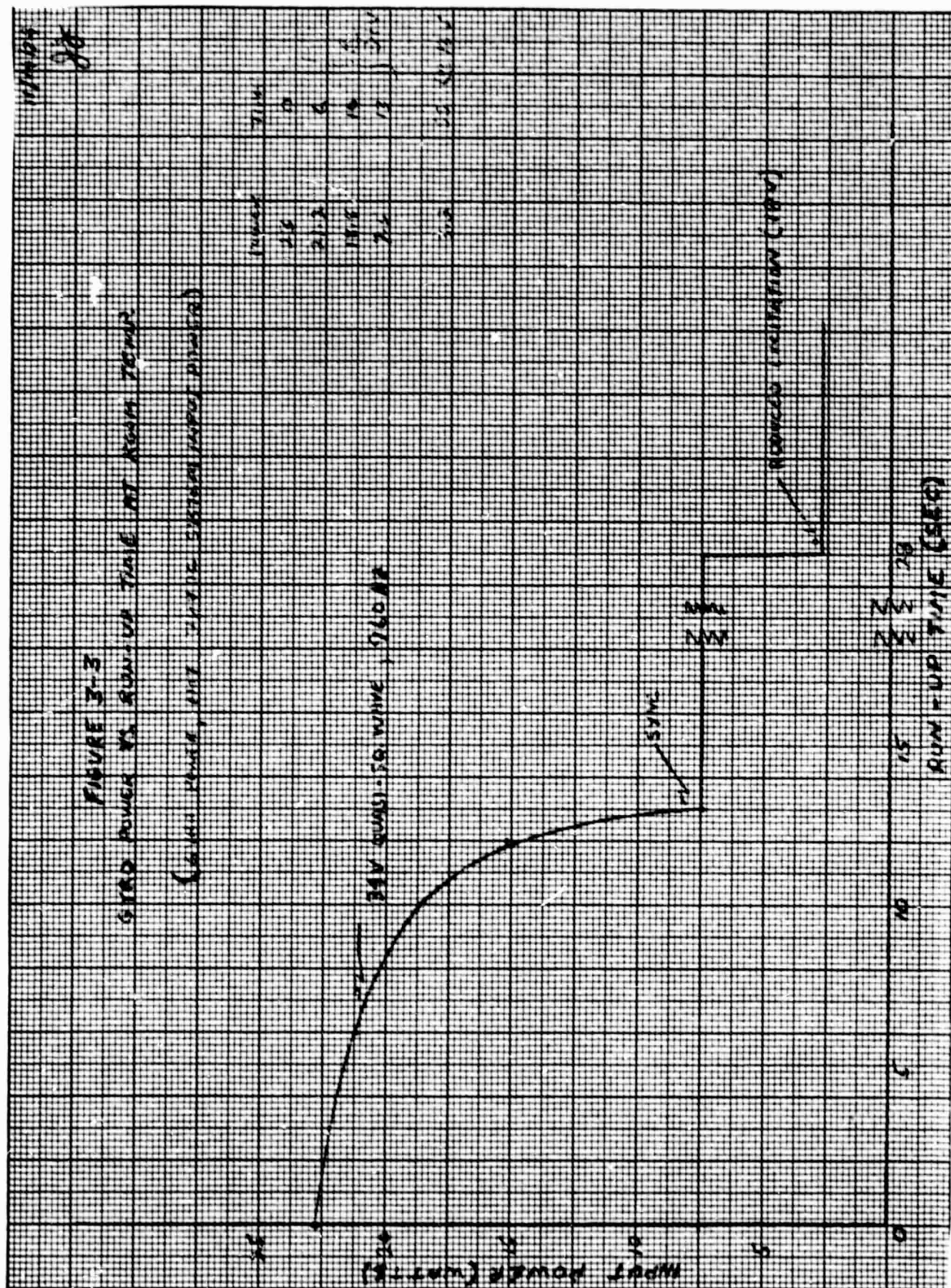
### 3.3 Mode Control Flexibility

The IRA mode options are discussed in the following sections.

#### 3.3.1 Hold/Slew vs. Rate

The gyros may be commanded through the serial link to be in either the hold/slew mode or rate mode individually.





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The matrix amplifiers are set to the hold/slew gain when any gyro is commanded to the hold/slew mode. There are two sets of matrix amplifiers, one associated with the use of each common electronics. Analog rate from gyros 1, 3, 5 is used in conjunction with the matrix amplifiers in common electronics "A". Rate from gyros 2, 4, 6 is used to generate body rate when common electronics "B" is used.

#### 3.3.2 Gyro On/Off

Any gyro may be commanded on or off individually through the common electronics via the serial link. This control is independent of the associated gyro heater.

#### 3.3.3 Heater Control

The gyro heaters have two power ranges; 4.5 and 12 watts. The heaters consist of two windings a 4.5 watt winding and a 7.5 watt winding. The 4.5 and 12 watt ranges are determined by opening or closing a latch device in series with the 7.5 watt winding. The system is designed such that the heaters can be individually switched to the 4.5 watt state or the 12 watt state.

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#### 3.3.4 System On/Off

The IRA System can be deenergized completely only through the spacecraft buss relays (eight). These relays override the common electronics control and in the case of buss no. 7 and no. 8 remove all power from the common electronics.



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The on/off mechanization is as follows:

Busses 1-6 are energized to apply heater power to the gyro heaters and to make power available to the gyro power supplies. The gyro power supplies (and the rate sensors) are not energized until the common electronics is powered (by buss no. 7 or no. 8) and commands issued. If the entire system was on and the buss supplying the common electronics was switched off, all power would be removed from all rate sensors except heater power. The heater would be switched to the 4.5 watt state if it was originally in the 12 watt state.

If the common electronics was energized first and a command issued to energize a gyro and then the gyro buss energized, the gyro would come up in the state dictated by the common electronics.

It is possible to command both common electronics to the on condition simultaneously. If this occurs an interlock is provided that disables both frequency counters and essentially shuts the system off.

No damage will occur within the IRA but all information will be invalid.

### 3.3.5 Bias Compensation Control

Matrix bias compensation is performed by commanding appropriate bits through the Command Decoder interface. Three bits are reserved for matrix axis address, which allows each body axis to be biased individually. Ten bits are used for data, the format being 2's complement.

### 3.3.6 Command Word Structure

All the serial commands are derived from one 37 bit serial link. The IRA contains a 33 bit shift register thus accepting only bits 5-37. Table 3-1 defines the bit assignments. Bits 35-37 contain the address for bias compensation routing. Bits 25-34 contain the bias data. Bit 24 is a control bit or qualifier bit. When this bit is a "1" it will activate bit positions 5-23; when it is a "0" it will activate bits 25-37. The qualifier allows commands to be stored without having to command the same sections of a word repeatedly.

Bits 11-16 control the gyro on/off condition. Bits 5-10 are used for mode control, a "1" being Hold/Slew, a "0" identifying rate. Bits 17-22 are used to command the heaters to either the 4.5 or 12 watt state. BIT 23 commands the rate cold gain state for any gyro in the rate mode.

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TABLE 3-1  
COMMAND BIT ASSIGNMENT

<u>BIT NO.</u>	<u>FUNCTION</u>	<u>STATE</u>
37	Bias Address, Pitch	"1"=Active
36	Bias Address, Roll	"1"=Active
35	Bias Address, Yaw	"1"=Active
34	Bias Data LSB	0.05 arc sec/bit weighting
33	Bias Data	
32	Bias Data	
31	Bias Data	
30	Bias Data	
29	Bias Data	
28	Bias Data	
27	Bias Data	
26	Bias Data	
25	Bias Data MSB	
24	Qualifier Bit	"0"=Bias Information "1"=Command Change
23	Rate Cold Mode	"1"=On
22	Gyro No. 1 Heater Hi/Lo	"1"=12 Watt State
21	Gyro No. 2 Heater Hi/Lo	"1"=12 Watt State
20	Gyro No. 3 Heater Hi/Lo	"1"=12 Watt State
19	Gyro No. 4 Heater Hi/Lo	"1"=12 Watt State
18	Gyro No. 5 Heater Hi/Lo	"1"=12 Watt State
17	Gyro No. 6 Heater Hi/Lo	"1"=12 Watt State
16	Gyro Channel No. 1 On/Off	"1"=On
15	Gyro Channel No. 2 On/Off	"1"=On
14	Gyro Channel No. 3 On/Off	"1"=On
13	Gyro Channel No. 4 On/Off	"1"=On
12	Gyro Channel No. 5 On/Off	"1"=On
11	Gyro Channel No. 6 On/Off	"1"=On

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TABLE 3-1 COMMAND BIT ASSIGNMENT (Continued)

<u>BIT NO.</u>	<u>FUNCTION</u>	<u>STATE</u>
10	Mode Control Gyro No. 1, Hold-Slew/Rate	"1"=Hold/Slew
9	Mode Control Gyro No. 2, Hold-Slew/Rate	"1"=Hold/Slew
8	Mode Control Gyro No. 3, Hold-Slew/Rate	"1"=Hold/Slew
7	Mode Control Gyro No. 4, Hold-Slew/Rate	"1"=Hold/Slew
6	Mode Control Gyro No. 5, Hold-Slew/Rate	"1"=Hold/Slew
5	Mode Control Gyro No. 6, Hold-Slew/Rate	"1"=Hold/Slew
4	Not Used	
3	Not Used	
2	Not Used	
1	Not Used	

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### 3.3.7 Summary of Options

- a) The rate sensors may be turned on and off independently through the IRA common electronics.
- b) The rate sensors may be turned off independently through the spacecraft switched +28V lines.
- c) The common electronics is energized through separate buss lines. No internal protection is provided against energizing both common electronics simultaneously.
- d) Gyro mode selection is individual.
- e) Heater mode (hi/lo) is individual.
- f) Heaters may be operated without common electronics on (low heater only).
- g) Duty cycle of heaters can be switched by switching the heaters from hi to lo or vice versa.
- h) Many combinations of active rate sensors plus gyro heaters exist that will not violate the total power requirement.

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#### 4.0 REDUNDANCY ANALYSIS

The IRA, as designed, has extremely reliable piece parts and adequate redundancy to fulfill the IUE mission for the minimum three year period. Furthermore, the reliability prediction (Section 5.0) indicates an excellent five year capability.

This analysis will identify the major redundant functions and show how they interact to provide the necessary reliability. The analysis will be updated periodically to include secondary effects and insure that no single point failures exist. To date, no single point failures have been identified.

##### 4.1 Input Power

Power to the IRA system is transmitted on eight separate busses; each buss with a redundant high wire and a total of four grounds. Each of busses 1-6 supports one gyro electronics, one gyro and one gyro heater. Busses 7 and 8 supply power to the common electronics.

Since the common electronics sections (two) are powered from separate busses and the six rate sensors powered from separate busses, there exists no single point failure in the input power scheme.

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#### 4.2 Command/Control

As was mentioned in previous sections the IRA has redundant sets of common electronics. These electronics receive input commands from two separate Command Decoders. These commands use interface circuitry which isolate one Command Decoder from the other and allow either a failed high or low condition without affecting the addressing capability (see figure 4-1).

Output data is buffered, thus eliminating a failed low condition from inhibiting the redundant output. A failure internal to the common electronics would necessitate a switch to the redundant set.

Figure 4-2 shows the functional partitioning of the IRA into electronic card types and the functions contained on each card. Every electronic card is identical to at least one other electronic card or section on that card. Total redundancy is present.



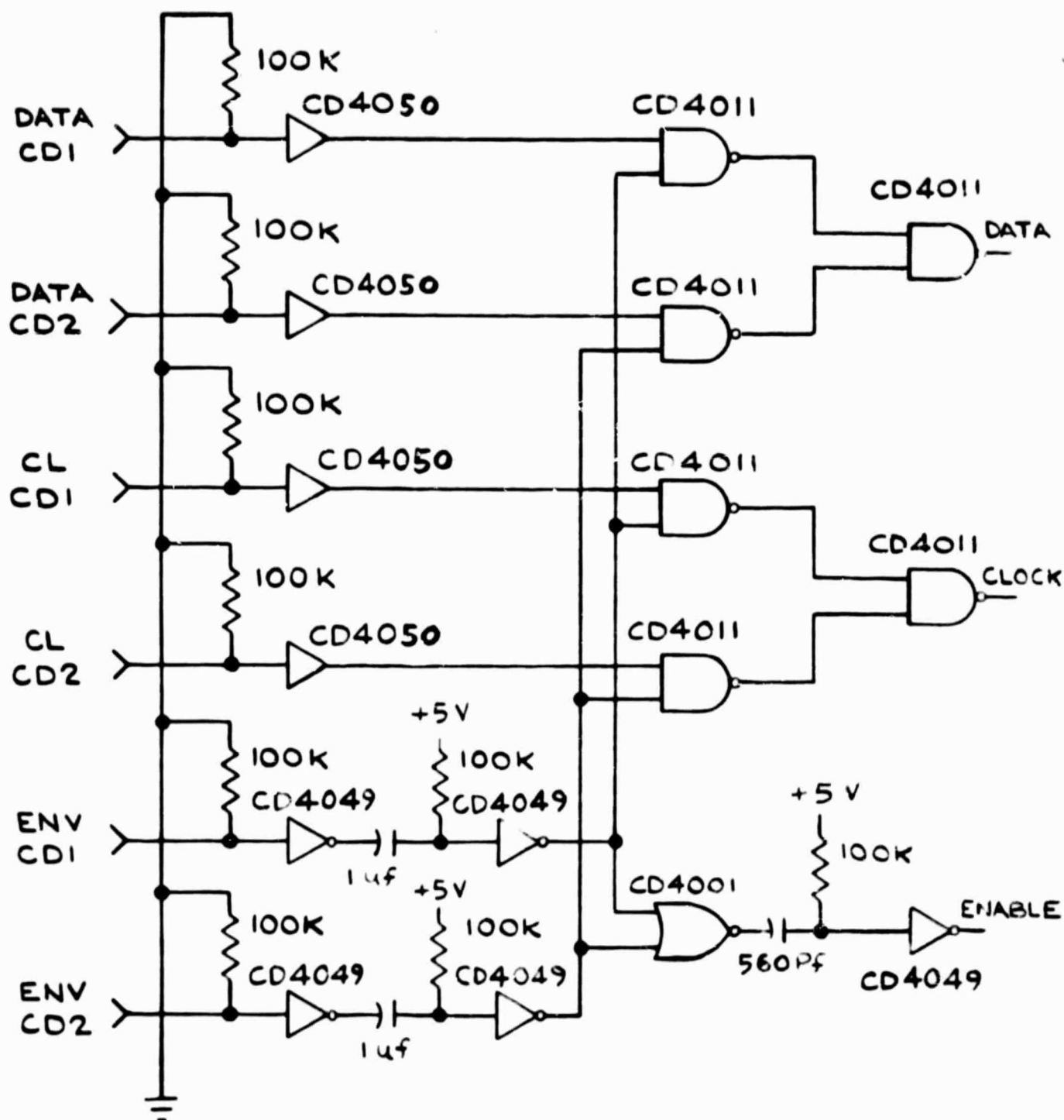
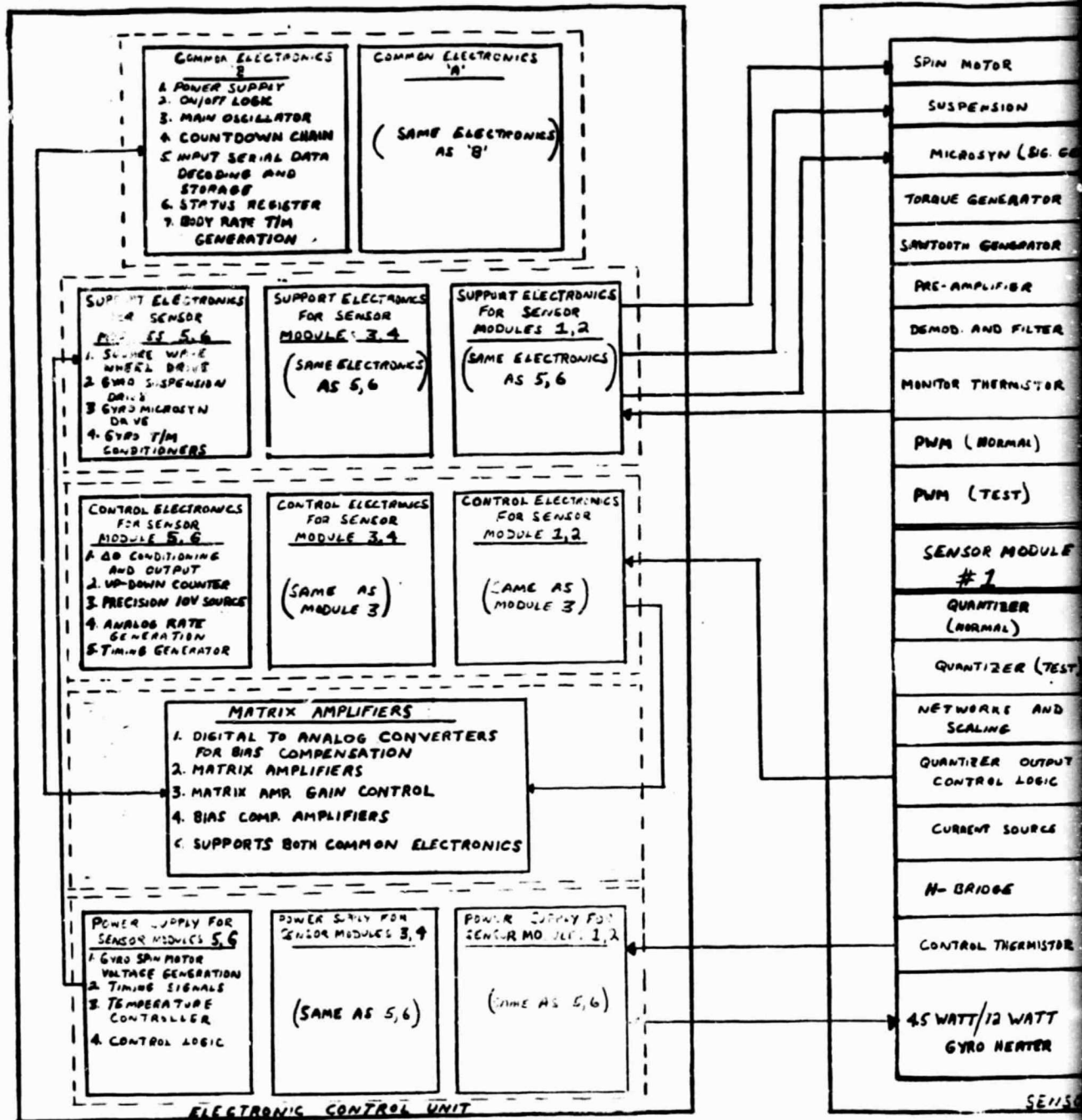


FIGURE 4-1

# COMMAND DECODER RECEIVER CIRCUIT



**SOLDOUT FRAME**

MF	REVISIONS				
ZONE	LYR	DESCRIPTION	DATE	APPROVED	



**FIGURE 4-2**

**FOLDOUT FRAME**

DN CHR ENGR LOG MVT REL APPD	THE BENDIX CORPORATION  NAVIGATION & CONTROL DIVISION TETTERBORO, NEW JERSEY, U.S.A.	
CONTRACT NO	IUE/IRA FUNCTIONAL PARTITIONING DIAGRAM	
APPROVAL	SIZE D	CODE IDENT NO. 19315
API POVAL	SCALE	SHEET

#### 4.3 Rate Sensor and Supporting Electronics

The IRA contains six rate sensors. A minimum of three is required to support the mission. The common electronics can address any rate sensor in any sequence. Each rate sensor heater has two ranges and can operate both open loop and closed loop.

Each rate sensor has a redundant, buffered digital  $\Delta\epsilon$  output. One is designated for transmission to DMU 'A', one to DMU 'B'. The output circuitry allows the DMU to address any gyro in any sequence. A failed gyro output or DMU address will not inhibit function of the redundant items.

#### 4.4 Common Electronics/Rate Sensor Support Electronics Interface

The remaining area to be addressed is the interface between the common electronics and the rate sensor support electronics. All logic level interfaces are "OR" type interfaces. All voltage excitation interfaces have diode protection that will prevent a shorted line from inhibiting use of the other common electronics. A failed high line is corrected by switching the associated rate sensor or common electronics to off. No single point failure exists in the interface between the common electronics and the rate sensors.

## 5.0 RELIABILITY ANALYSIS

### 5.1 Reliability Prediction Results

The results of the preliminary reliability prediction, of the Inertial Reference Assembly (IRA) for the International Ultraviolet Explorer (IUE) are presented below:

<u>Probability of Survival (<math>P_s</math>)</u>	<u>Mission Time</u>
<u>All Parts</u>	<u>(t)</u>
$P_{s_1}' = 0.9652$	$t_1 = 26,280 \text{ hr}^*$
$P_{s_2}' = 0.8579$	$t_2 = 43,800 \text{ hr}^{**}$

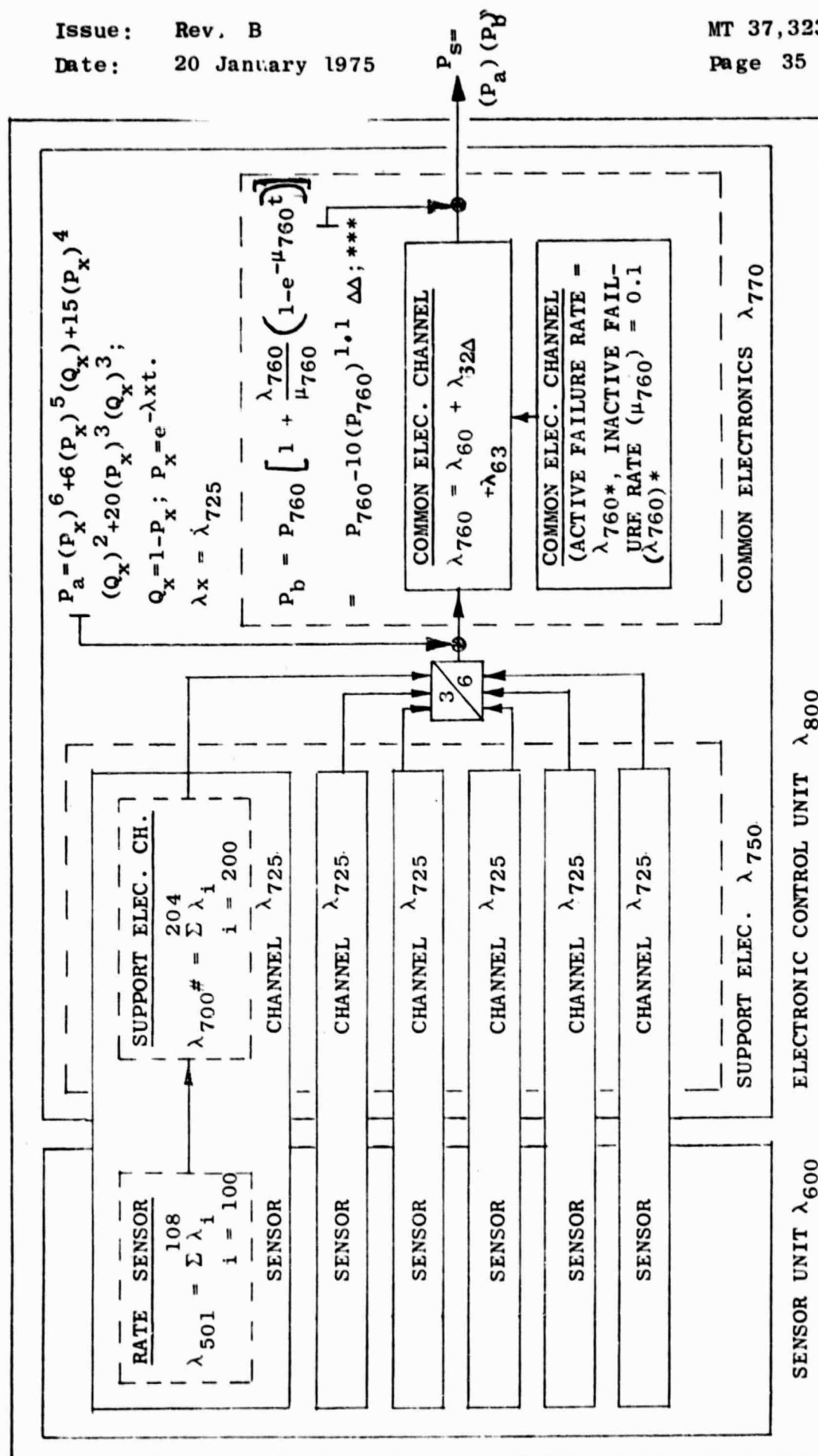
\*Three years

\*\*Five years

The IRA probabilities of survival tabulated above are based upon an orbital environment and an ambient temperature of  $120^{\circ}\text{F}$  ( $48.9^{\circ}\text{C}$ ), except for the Gyros which will be controlled to  $135^{\circ}\text{F}$  ( $57.2^{\circ}\text{C}$ ).

### 5.2 Reliability Block Diagram and Mathematical Model

The reliability block diagram and the associated mathematical model are depicted in Figure 5-1. Details of the analysis may be found in the DRL Reliability Report (GSD/RM 75-18, January 17, 1975).



INERTIAL REFERENCE ASSEMBLY  $\lambda_{900}$

FIGURE 5-1

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## 6.0 PERFORMANCE SUMMARY

Table 6-1 is a summary of performance characteristics of the IRA system and the GSFC specification values. The table is self-explanatory. The IRA capabilities meet or exceed the specification values in all areas.

## 7.0 WEIGHT SUMMARY

The IRA weight breakdown is shown in Table 7-1. The total system weight is 48.35 pounds.



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TABLE 6-1

IRA PERFORMANCE CAPABILITY SUMMARY

<u>PARA.NO.</u>	<u>PARAMETER</u>	<u>SPEC. VALUE</u>	<u>IRA CAPABILITY</u>
3.3.1	Integrated Rate Output	-	-
3.3.1.1	Pulse Weight	0.01 - 0.1 $\overline{\text{sec}}$ /pulse (Hold/Slew)	0.01 $\overline{\text{sec}}$ /pulse (H) 0.30 $\overline{\text{sec}}$ /pulse (R)
3.3.1.2	Range	$\pm$ 600 $\overline{\text{sec}}$ /sec (Hold/Slew)	$\pm$ 672 $\overline{\text{sec}}$ /sec
3.3.1.3	Bandwidth	Gyro Time Constant <0.005 sec Loop Bandwidth >5 Hz	0.0011 sec 7.5 Hz
3.3.1.4	Scale Factor Linearity	$\pm$ 0.1%	$\pm$ 0.05%
3.3.1.5	Scale Factor Stability	$\pm$ 0.01% over 35 days (min.)	$\pm$ 0.01%
3.3.1.6a	Non g-Sensitive Bias Drift	$\pm$ 5.0 $\overline{\text{sec}}$ /sec (max.)	$\pm$ 3.0 $\overline{\text{sec}}$ /sec (max)
	Variation of Non g-Sensitive Drift Over Test	0.5 $\overline{\text{sec}}$ /sec	0.25 $\overline{\text{sec}}$ /sec
3.3.1.6b	g-Sensitive Drift	$\pm$ 10.0 $\overline{\text{sec}}$ /sec/g (max)	$\pm$ 0.75 $\overline{\text{sec}}$ /sec/g
	Variation of g-Sensitive Drift over Test	1.0 $\overline{\text{sec}}$ /sec/g	$\pm$ 0.15 $\overline{\text{sec}}$ /sec/g
3.3.1.7	Bias Drift Stability	$\pm$ 0.01 $\overline{\text{sec}}$ /sec over 35 days (min.)	$\pm$ 0.01 $\overline{\text{sec}}$ /sec
3.3.1.8	Short-Term Attitude Noise	1 $\overline{\text{sec}}$ over 1st 5 min. 2 $\overline{\text{sec}}$ over 30 min	< 1 $\overline{\text{sec}}$ < 2 $\overline{\text{sec}}$
	Variation on Consecutive Date Points	0.2 $\overline{\text{sec}}$	0.1 $\overline{\text{sec}}$
3.3.2	Analog Rate Output	-	-
3.3.2.1	Range	Linear over -5 to +5VDC	Same as spec value
	Scale Factor	Rate Mode      Hold/Slew Mode (VDC/deg/sec)      (VDC/ $\overline{\text{sec}}$ /sec)	Same as spec value
		Pitch/Yaw/ 1.0      0.050 Roll      1.0      0.050	
3.3.2.2	Bias Compensation (Hold/Slew Mode)	$\pm$ - $\overline{\text{sec}}$ /sec with reso- lution of 0.05 $\overline{\text{sec}}$ /sec and 0.60 $\overline{\text{sec}}$ /sec for roll	$\pm$ 25 $\overline{\text{sec}}$ /sec (X12) 0.05 $\overline{\text{sec}}$ /sec 0.60 $\overline{\text{sec}}$ /sec f

FOLDOUT FRAME

TABLE 6-1

PERFORMANCE CAPABILITY SUMMARY

<u>VALUE</u>	<u>IRA CAPABILITY</u>	<u>BASIS FOR ESTIMATE</u>
	-	-
sec/pulse	0.01 <u>sec</u> /pulse (Hold/Slew)	Design Analysis and 64 PM RIG Rate
	0.30 <u>sec</u> /pulse (Rate)	Sensor experience
	$\pm 672 \sqrt{\text{sec/sec}}$	Design analysis
stant	0.0011 sec	Design analysis
h > 5 Hz	7.5 Hz	
	$\pm 0.05\%$	64 PM RIG Rate Sensor experience
35 days	$\pm 0.01\%$	Design analysis and 64 PM RIG Rate
		Sensor experience
(max.)	$\pm 3.0 \sqrt{\text{sec/sec}}$ (max.)	64 PM RIG Rate Sensor experience
	0.25 <u>sec</u> /sec	64 PM RIG Rate Sensor experience
sec/g (max)	$\pm 0.75 \sqrt{\text{sec/sec/g}}$	64 PM RIG experience
	$\pm 0.15 \sqrt{\text{sec/sec/g}}$	64 PM RIG experience
sec over	$\pm 0.01 \sqrt{\text{sec/sec}}$	64 PM RIG Rate Sensor experience
at 5 min.	$< 1 \sqrt{\text{sec}}$	64 PM RIG Rate Sensor experience
0 min	$< 2 \sqrt{\text{sec}}$	64 PM RIG Rate Sensor experience
	0.1 <u>sec</u>	64 PM RIG Rate Sensor experience
	-	-
-5 to +5VDC	Same as spec values	Design Analysis
Hold/Slew	Same as spec values	Design Analysis
Mode		
(VDC/ <u>sec</u> /sec)		
0.050		
0.050		
with reso-	$\pm 25 \sqrt{\text{sec/sec}}$ (X12 in Roll)	Design Analysis
0.05 <u>sec</u> /sec	0.05 <u>sec</u> /sec and	
/sec for roll	0.60 <u>sec</u> /sec for roll	

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TABLE 7-1  
IUE/IRA WEIGHT SUMMARY

<u>Item</u>	<u>Weight (lbs.)</u>
<u>Sensor Unit</u>	
Mechanical Structure	4.30
Optical Cube and Alignment Bar	0.15
Mount	1.60
<u>ITEM</u>	
<u>Sensor Unit</u>	
Rate Sensors	
Six Gyros @ 1.70 lb each	10.20
Six PRL Elect., Covers and Cables	
@ 1.43 each	<u>8.6</u>
Sensor Unit Total =	26.15
<u>Electronic Control Unit</u>	
Mechanical Structure	4.10 +
Connectors	0.44
EMI Modules	2.00
Electronics (12 Cards)	9.96
Back Panel Wiring	1.00
Miscellaneous Hardware	<u>0.80</u>
Electronic Control Unit Total =	22.2
System Total =	<u>48.35</u>

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## 8.0 POWER SUMMARY

### 8.1 Detailed Power Breakdown

Table 8-1 describes the detailed power breakdown within the IRA. The nominal operating power required for the system is 74.2 watts. This figure includes six rate sensors on, one common electronics on and the gyro heaters drawing an average of 2.22 watts each.

It should be noted that the actual total power consumed by the IRA is dependent upon the temperature of the rate sensors, the number of rate sensor energized and the mode of the rate sensor heater (hi or lo).

**TABLE 8.1**  
**DETAILED POWER BREAKDOWN**

<u>ITEM</u>	<u>POWER (WATTS)</u>	
<u>RATE SENSOR</u>		
GYRO TORQUER	0.150	
GYRO WHEEL	3.200	
GYRO SUSPENSION	0.185	
GYRO MICROSYN	0.002	
PRE-AMP	0.120	
DEMODULATOR	0.100	
GAIN CHANGE	0.010	
SAWTOOTH AND QUANT.	0.270	
TORQUER CURR. SOURCE	0.800	
TORQUER H-BRIDGE	<u>0.550</u>	
	5.387	SUBTOTAL - ONE RATE SENSOR
		x 6 = 32.328
<u>SUPPORT ELECTRONICS</u>		
WHEEL DRIVE	0.680	
SYNC DETECTOR	0.010	
TEMP. MON.	0.025	
MOTOR CURR. MON.	0.010	
MICROSYN DRIVE	0.150	
SUSPENSION DRIVE	0.480	
FILTER	<u>0.050</u>	
	1.405	SUBTOTAL - ONE CHANNEL
		x 6 = 8.430
<u>CONTROL ELECTRONICS</u>		
VOLTAGE REF.	0.45	
PWM TO DC CONV.	0.050	
INVERTER	0.050	
T/M CIRCUITS	0.010	
LOGIC	<u>0.010</u>	
	0.570	SUBTOTAL - ONE CHANNEL
		x 6 = 3.42

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TABLE 8.1  
POWER BREAKDOWN

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<u>ITEM</u>	<u>POWER (WATTS)</u>
<u>GYRO PWR SUPPLY</u>	
DC POWER SUPPLY	1.280
TEMP. CONTROLLER	<u>0.200</u>
	1.480
	SUBTOTAL - ONE CHANNEL
	x 6 = 8.880
<u>MATRIX AMPLIFIER</u>	
LOGIC	}
D/A CONVERTER	
AMPL	
	1.54
<u>COMMON ELECTRONICS</u>	
T/M FUNCTIONS	0.030
LOGIC	0.200
OSCILLATOR	0.100
POWER SUPPLY	<u>0.230</u>
	0.560
RFI FILTERS (6)	1.660
HEATER CONTROL CKT (6)	4.068
NOM. HEATER PWR (6)	13.32

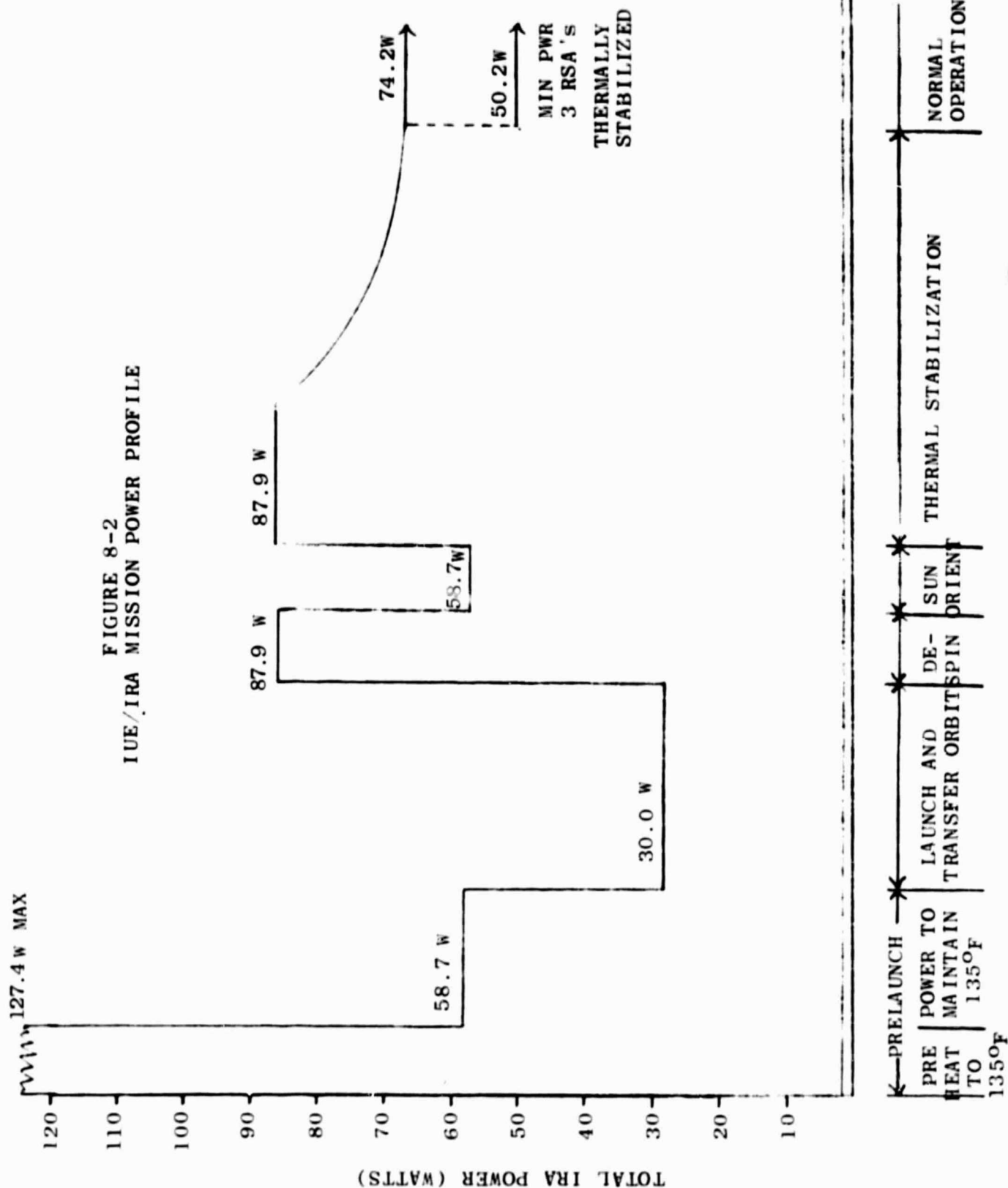
SYSTEM OPERATING POWER = 74.2 WATTS  
(6 GYROS ON, TEMP STABILIZED)

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FIGURE 8-2  
IUE/IRA MISSION POWER PROFILE





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Breakdown of the total power numbers is as follows:

127.4 watt maximum - includes 72 watts heater power, 32 watts dissipation in 6 RSAs, 28 watts ECU power - represents the total power consumed if system is full on in the highest heater mode (used to obtain 135°F quickly during ground operation).

58.7 watts - heater power required to maintain 135°F on RSAs at 70°F ambient.

30.0 watts - maximum power available to the IRA during launch and transfer orbit.

87.9 watts - total power consumed with heaters in the 4.5 watt state, ECU and six RSAs 'on' and all RSAs below 135°F.

58.3 watts - total power consumed with heaters in the 4.5 watt state (all six 'on'), 1/2 ECU 'on' and three RSAs 'on'.

74.2 watts - steady state power consumption with six RSAs 'on'

50.2 watts - steady state power consumption with three RSAs 'on'.

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## 9.0 MECHANICAL CONFIGURATION SUMMARY

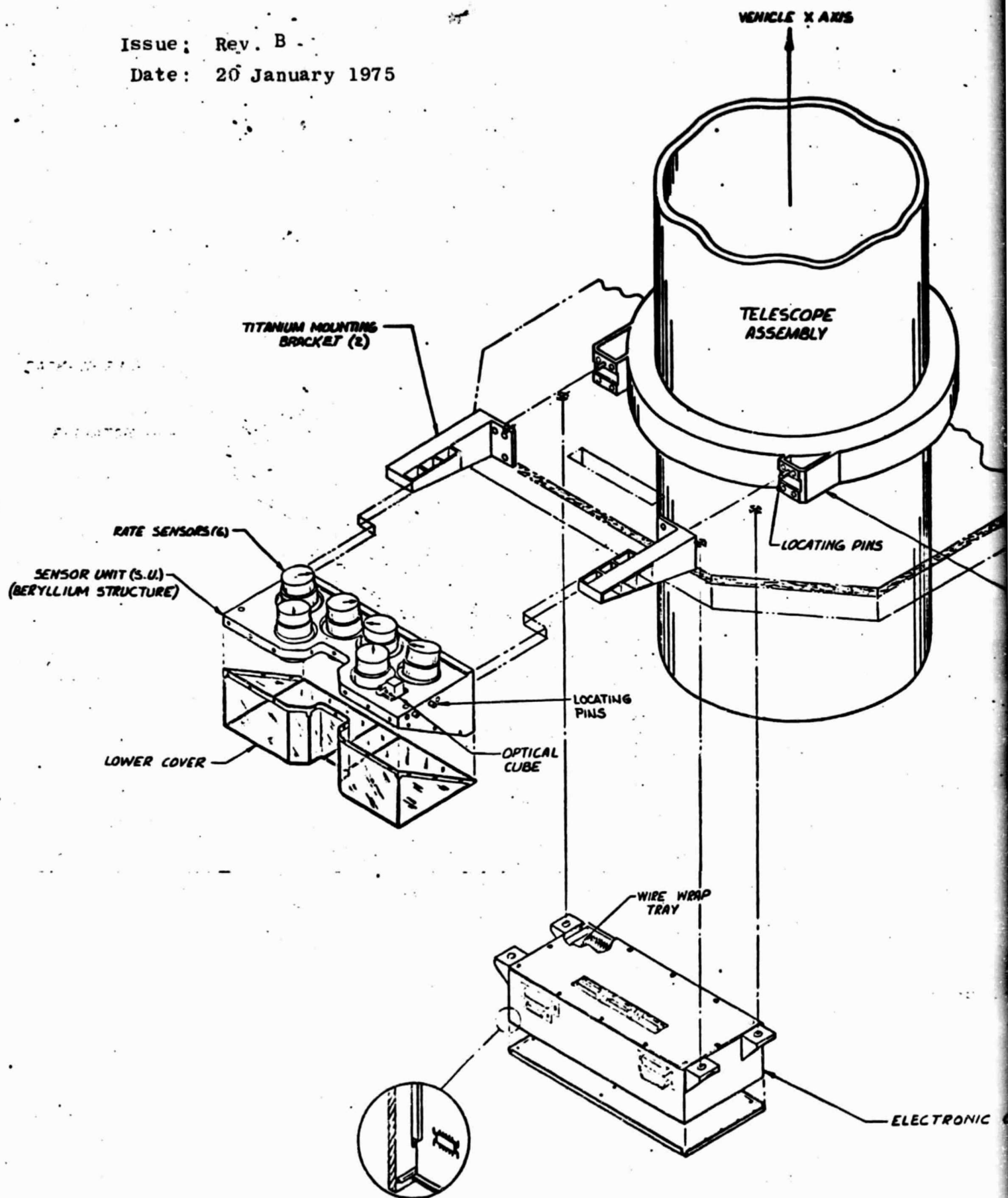
Figure 9-1 shows an exploded view of the IRA units illustrating the mounting arrangement to the telescope strong ring and honeycomb structure. The Sensor Unit mounts to the strong ring in a cantilever manner. A titanium mounting strut is used for strength and proper thermal characteristics. The lower cover of the Sensor Unit is an aluminum frame with aluminized mylar skin.

The cutout in the Sensor Unit is for passage of the six rate sensor cables to the Electronic Control Unit below. Each sensor cable is identical in pin assignment but contains different keying. By changing the keying each rate sensor will be interchangeable with the others.

Mounted below the Sensor Unit is the Electronic Control Unit. This unit contains six connectors for interface with the SU, three connectors for the S/C interface and one test connector.

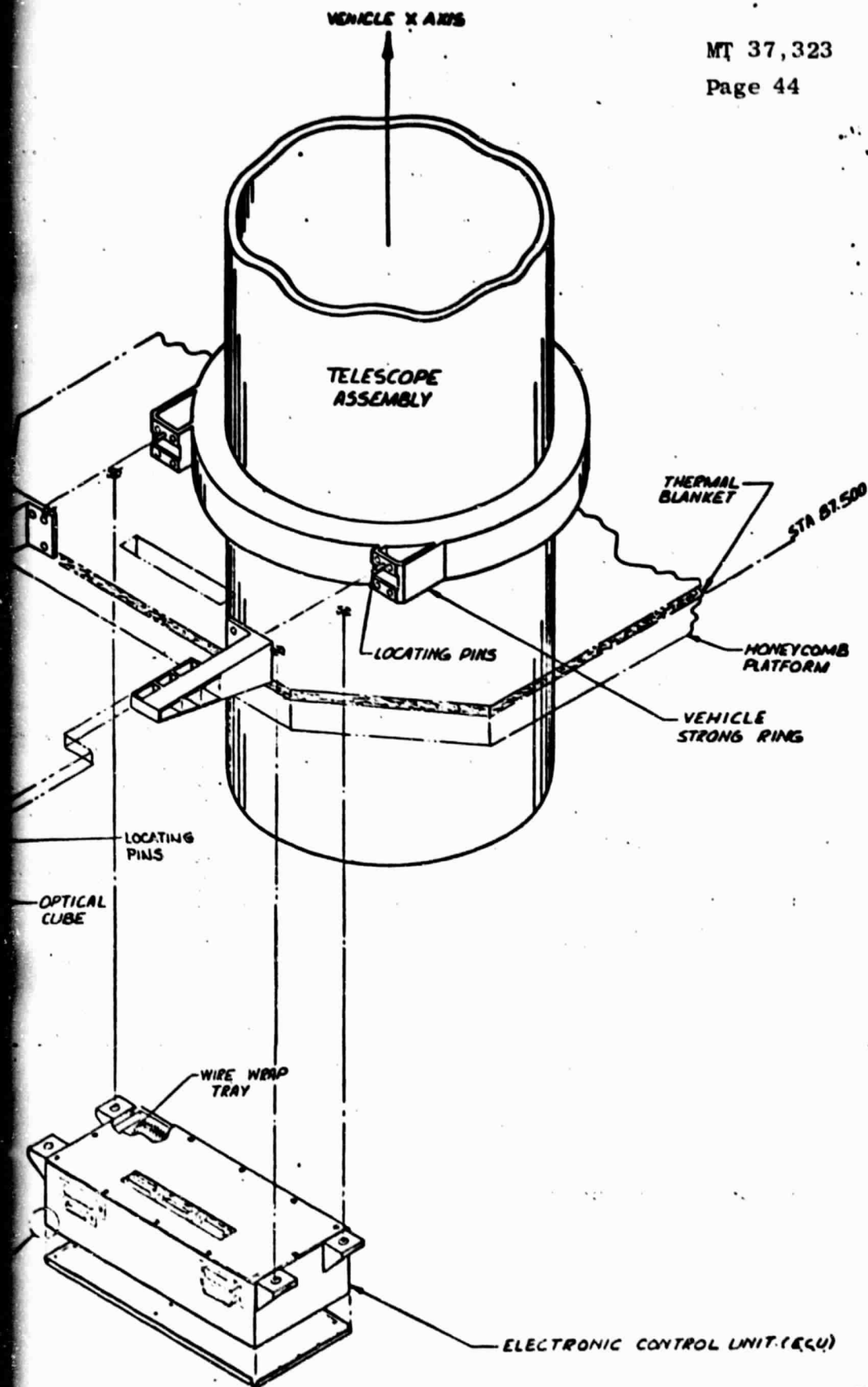
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FOLLOW-UP FRAME

IUE/IRA EXP



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IUE/IRA EXPLODED VIEW

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## 10.0 MECHANICAL INTERFACE

### 10.1 Sensor Package Mechanical Interface

Figure 10-1 defines the mechanical interface between the IUE/IRA Sensor Package and the IUE Strong Ring.

Eight (8) .250 bolts are used for mounting in the  $.261 \pm .006$  clearance holes.

Two (2)  $.2501 \pm .0000$  diameter locating pins will be used for location of the IRA Sensor Package. The pins used will be fabricated of 416 Corrosion Resistant Steel, and will have a lead-in angle for ease of installation. A 416 CRE pin with a .2500 diameter will sustain a shear load of 3600 pounds. Assuming no frictional force due to the tightening of the eight (8) mounting bolts, the worst case shear load at each pin would be 1600 pounds.

Detail dimensions and tolerances of the recommended pin are shown in Figure 10-3.

Since GSD has been advised by GSFC that the Strong Ring has been manufactured and contains the keyway as shown in Figure 10-1, the locating pin will be located in the thicker section of the Strong Ring rather than the geometric center of the mounting holes.

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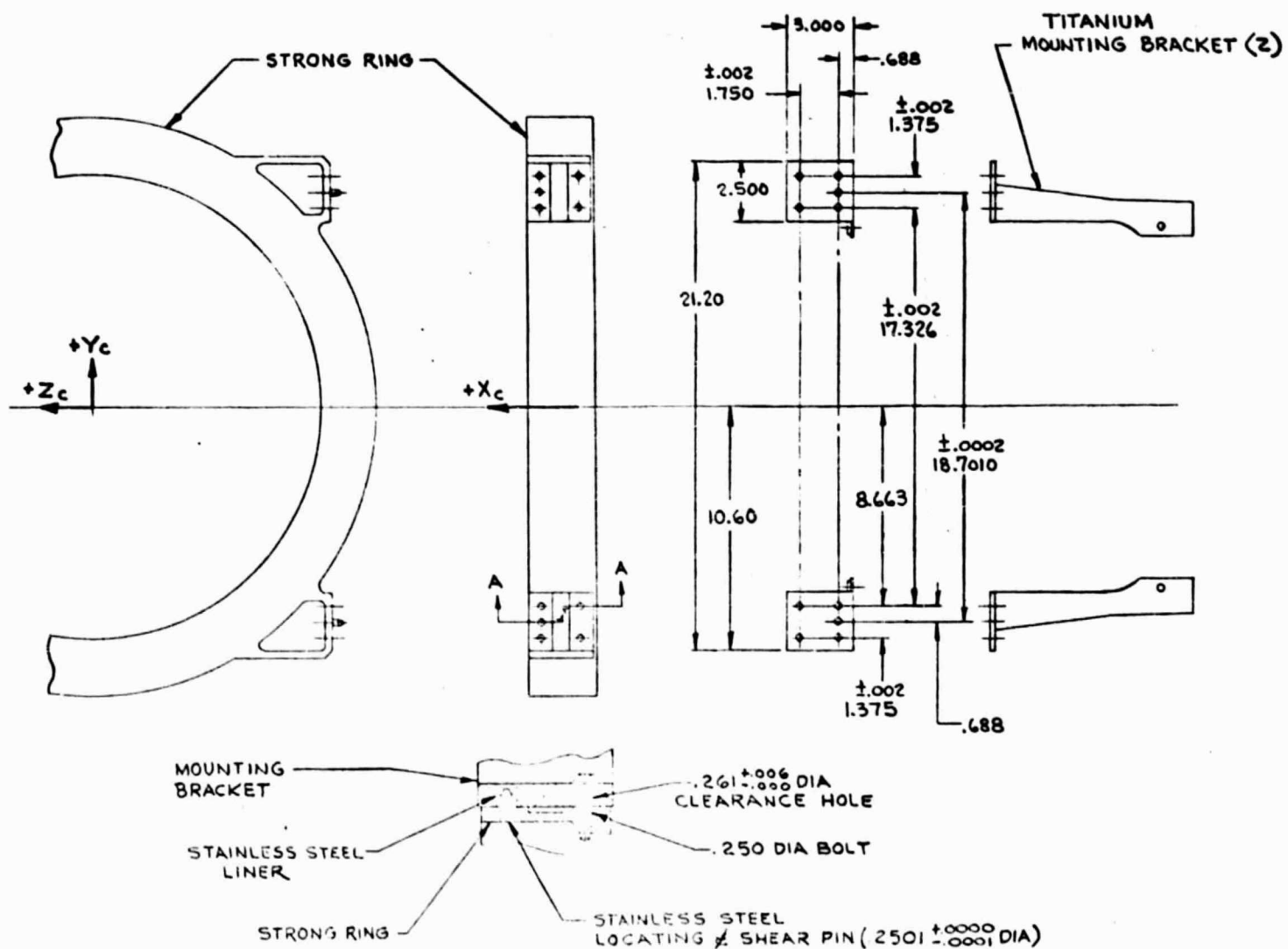


FIGURE 10-1

IUE/IRA MECHANICAL INTERFACE  
(SENSOR PACKAGE)

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10.1 (continued)

A recommended transfer tool for locating the holes in the IUE Strong Ring is shown in Figure 10-2. The transfer tool would be matched to the holes in the mounting ring and aligned to it within  $\pm .0002$  inches. Removable hardened steel bushings would be used for first drilling the holes in the Strong Ring and a second set for reaming to final size prior to installing the locating pins. Final hole size should be  $.2504 \begin{smallmatrix} + .0002 \\ - .0000 \end{smallmatrix}$  in the IRA to provide a fit of .0003 to .0006 loose; and  $.2496 \begin{smallmatrix} + .0002 \\ - .0000 \end{smallmatrix}$  to provide a fit of .0002 to .0005 tight in the strong ring.

The IRA Sensor Package mounts by the use of .250 bolts through clearance holes (.261 dia.) rather than tapped holes. This implies the use of washers, lockwashers and nuts on the other side of the Strong Ring (Ref. Figure 1).

Receipt of GSFC Drawing GE1172537 and conversations with GSFC has indicated that no mounting problem exists.



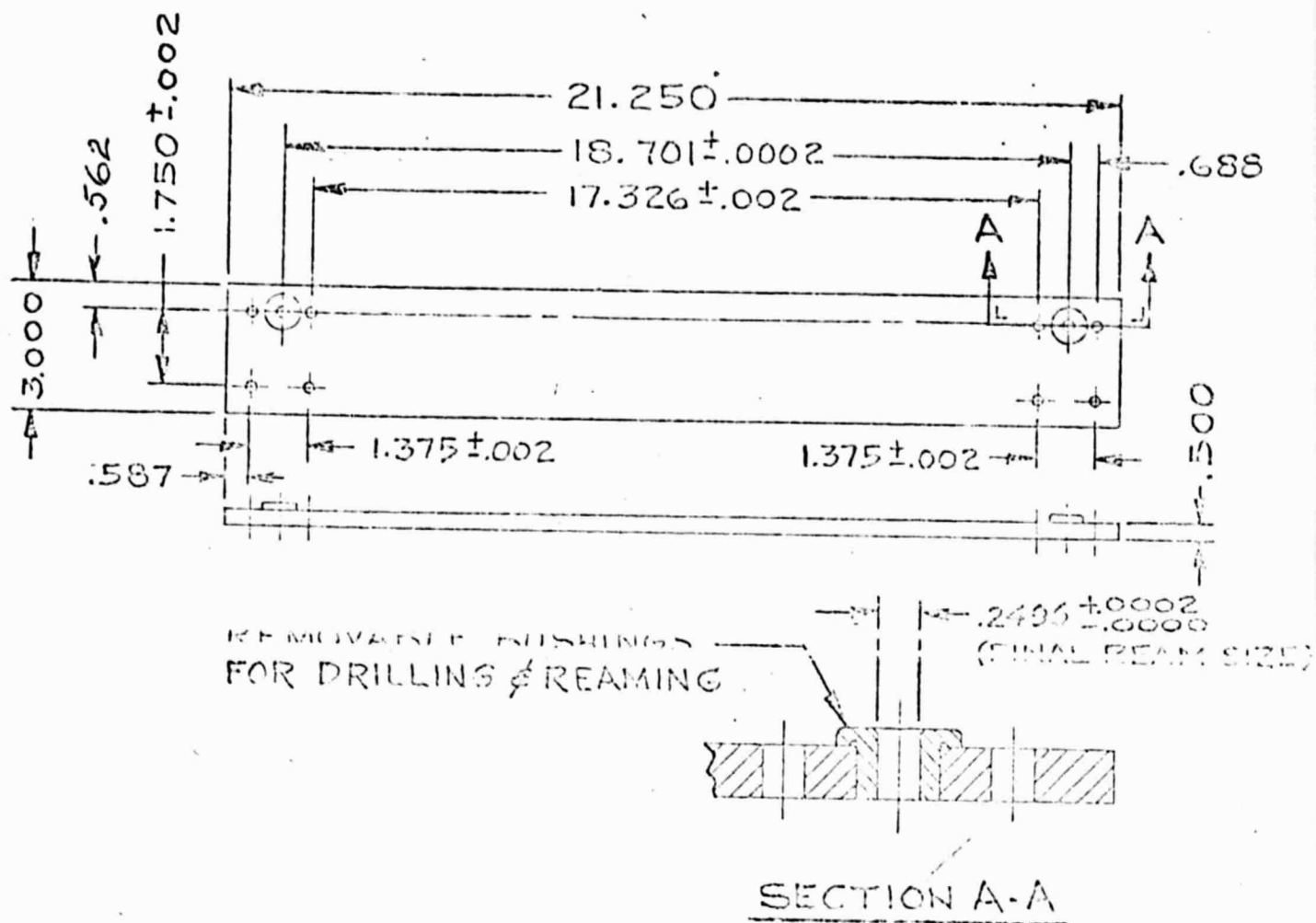


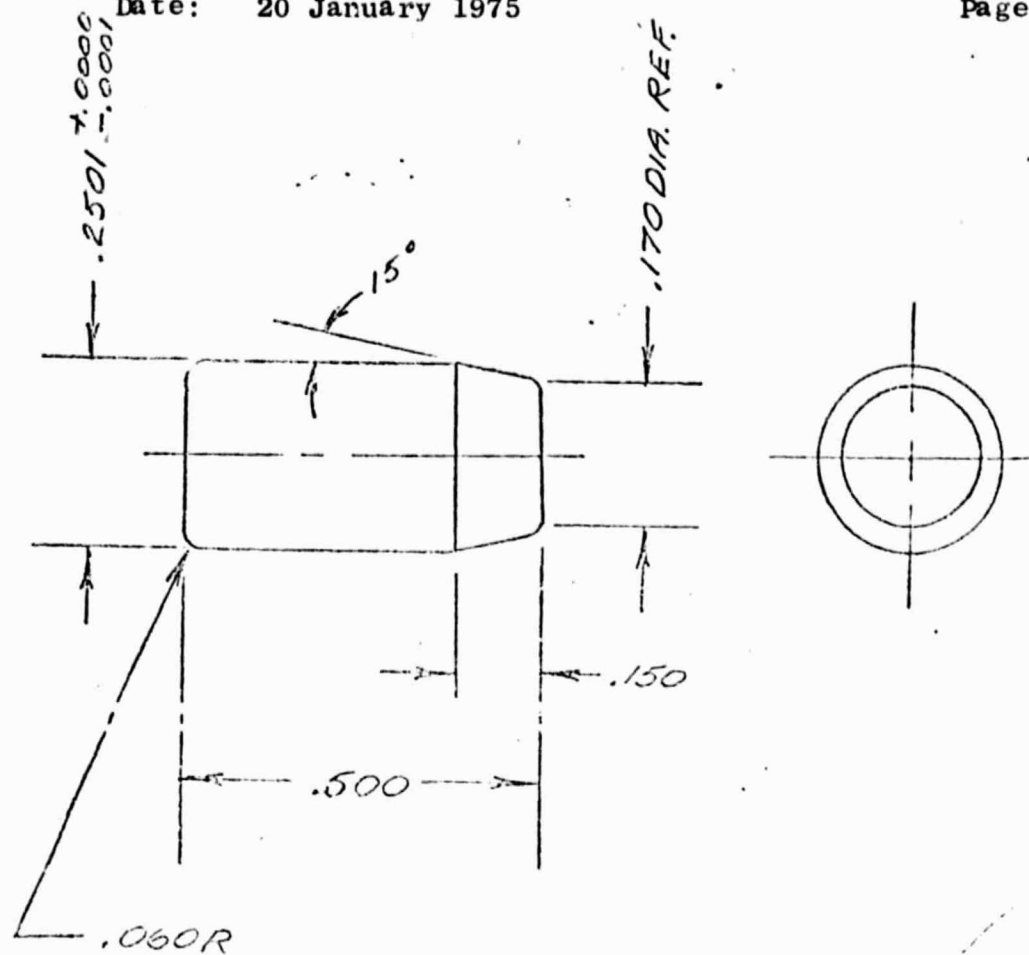
FIGURE 10-2  
TRANSFER TOOL CONCEPT

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RC-34-33

FIGURE 10-3

LOCATING PIN

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## 10.2 Electronic Control Unit Mechanical Interface

Figure 10-4 illustrates the mechanical interface and interconnect for the Sensor Unit and the Electronic Control Unit. This figure shows the mounting dimensions with respect to the Strong Ring Interface; the Sensor Unit above the upper honeycomb platform and the Electronics Unit mounted below. Each Rate Sensor mounted in the sensor unit is connected to the electronics unit directly by means of a cable originating at each individual rate sensor and terminating at the electronics control unit connector interface. A separate ECU connector is used for each rate sensor.

## 11.0 ELECTRICAL INTERFACE

### 11.1 Functional Interface

Figure 11-1 shows the basic electrical interface of the IRA boxes with each other and with the spacecraft. The spacecraft interface is two 78 pin connectors and one 26 pin connector. All power is on the 26 pin connector.



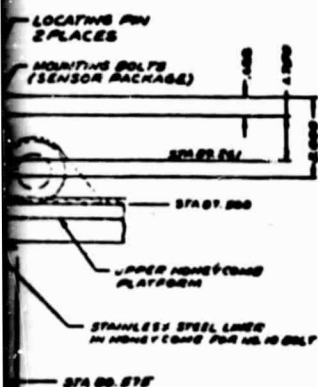
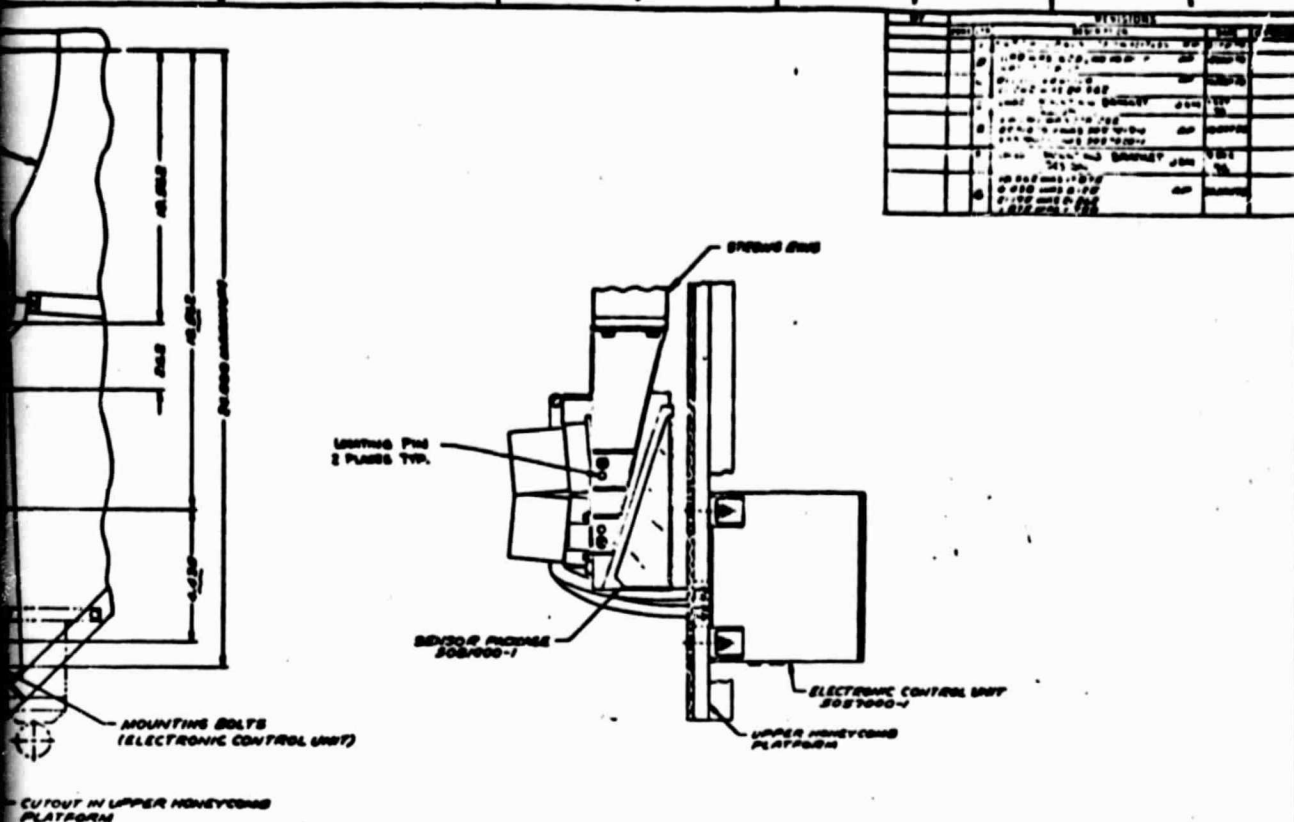


FIGURE 10-4

IUE/IRA SENSOR UNIT AND ELECTRONIC  
CONTROL UNIT INTERFACE

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1. PREPARED BY: [ ] 2. CHECKED BY: [ ] 3. APPROVED BY: [ ] 4. DATE: [ ]		5. PART NO.: [ ] 6. REV.: [ ] 7. QTY.: [ ] 8. UNIT: [ ]	
9. TITLE: [ ] 10. DESCRIPTION: [ ] 11. MATERIAL: [ ] 12. FINISH: [ ]		13. DRAWN BY: [ ] 14. CHECKED BY: [ ] 15. APPROVED BY: [ ] 16. DATE: [ ]	
17. PART NO.: [ ] 18. REV.: [ ] 19. QTY.: [ ] 20. UNIT: [ ]		21. TITLE: [ ] 22. DESCRIPTION: [ ] 23. MATERIAL: [ ] 24. FINISH: [ ]	

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The interface between the SU and ECU is by six 50 pin connectors, one for each rate sensor.

Also contained on the ECU is a 104 pin connector used strictly for test purposes. This connector will be capped for flight.

Figure 11-2 shows the IRA pin function diagram. The two 78 pin connectors were made to be functionally identical as were the six 50 pin rate sensor connectors.

#### 11.2 Detailed Electrical Interface

The IRA/Spacecraft electrical interface can be characterized by several input and output circuit types. These types are shown below. Table 11-1 details the electrical characteristics of each signal with reference to the circuit type.

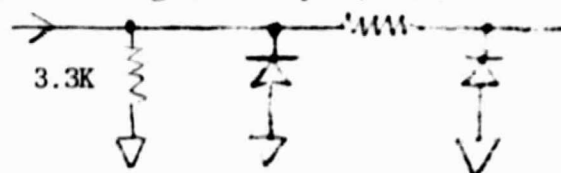
Type: B 1-6 - Power buss input, 28 VDC  $\pm$  2%, complex load ( $R = 62.2 \Omega$ )

B 7-8 - Power buss input, 28 VDC  $\pm$  2%, complex load ( $R = 509 \Omega$ )

DI-1 - Digital input, CMOS device 4050, 4049



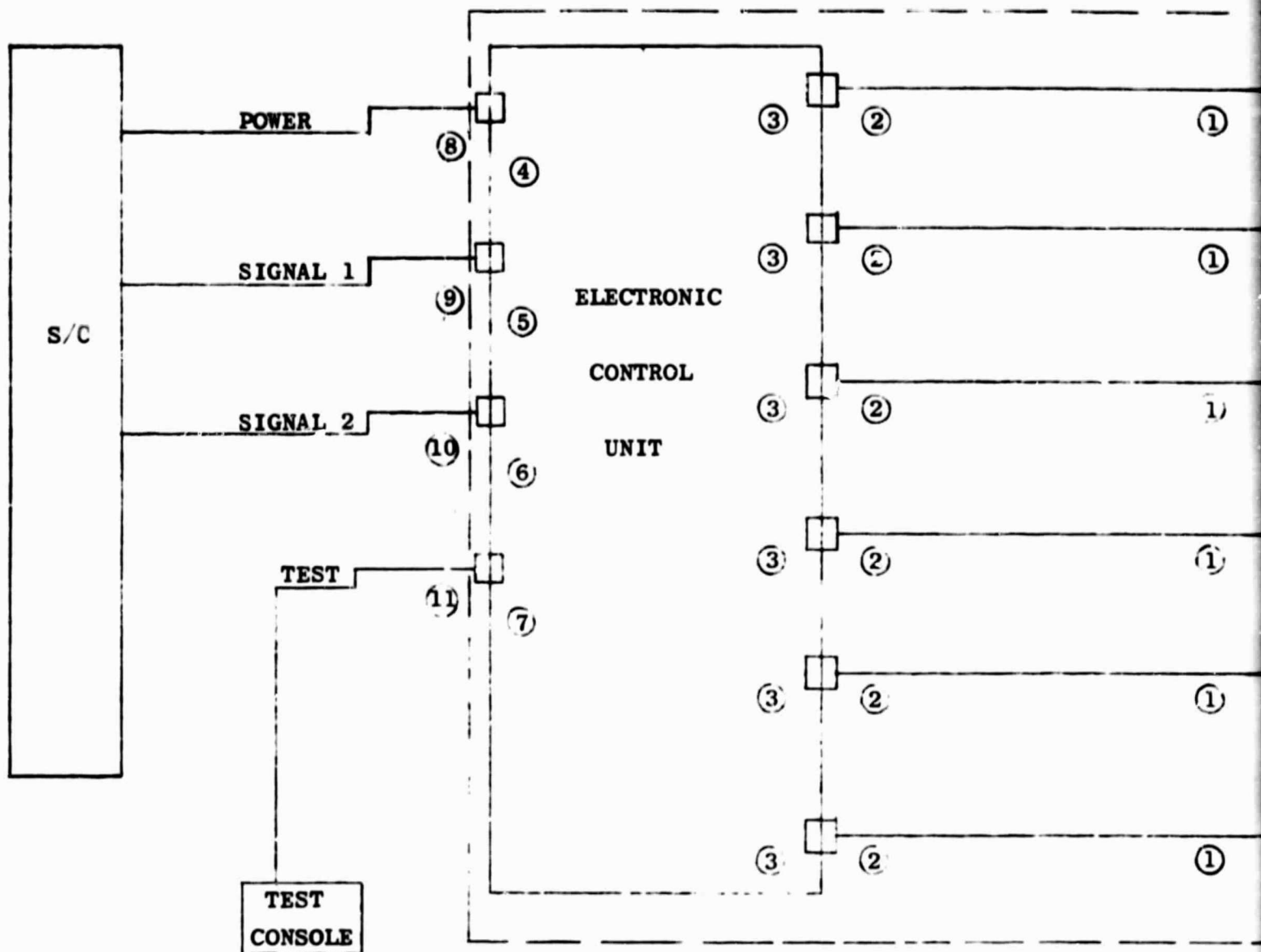
DI-2 - Digital input, CMOS device 4050, 4049



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# IUE/IRA SUBSYSTEM



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IUE/IRA SUBSYSTEM

		SENSOR UNIT
(2)	(1)	GYRO #1
(2)	(1)	GYRO #2
(2)	(1)	GYRO #3
(2)	(1)	GYRO #4
(2)	(1)	GYRO #5
(2)	(1)	GYRO #6

- (1) CONNECTIONS MADE  
INTERNAL TO GYRO MODULE
- (2) CANNON DDMAM50P  
(MIL M 24308/3-5) ALL  
KEYED DIFFERENTLY
- (3) CANNON DDMAM50S  
(MIL M24308/2-5) ALL  
KEYED W.R.T. 2
- (4) 311 P 407-2P-B-15
- (5) 311 P 407-5S-B-15
- (6) 311 P 407-5S-B-15 WITH  
DIFFERENT KEY FROM 5
- (7) 311 P 407-6S-B-15
- (8) 311 P 407-2S-B-15
- (9) 311 P 407-5P-B-15
- (10) 311 P 407-5P-B-15 WITH  
DIFFERENT KEY FROM 9
- (11) 311 P 407-6P-B-15

FIGURE 11-1

IUE/IRA FUNCTIONAL  
INTERFACE

FIGURE 11-1

FOLDOUT FRAME

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**GUIDANCE  
SYSTEMS  
DIVISION**



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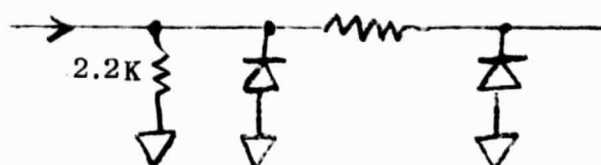
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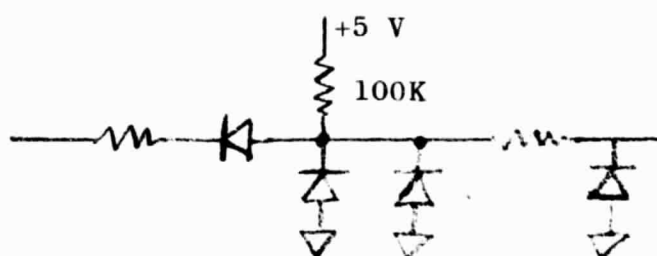
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11.2 (continued)

DI-3 - Digital input, CMOS device 4050, 4049



DI-4 - Digital input (test connector)



DO-1 - Digital output, CMOS driver device 4050, 4049, 1K resistor in series with output, can drive one  $T^2L$  load

AO-1 - Analog output,  $\pm 10$  VDC range, drive current = 22 ma, source impedance 1K ohms

AO-2 - Analog telemetry output, + 5.6 VDC to - 0.7 VDC range, source impedance 4.99 K ohms.

# FOLDOUT FRAME

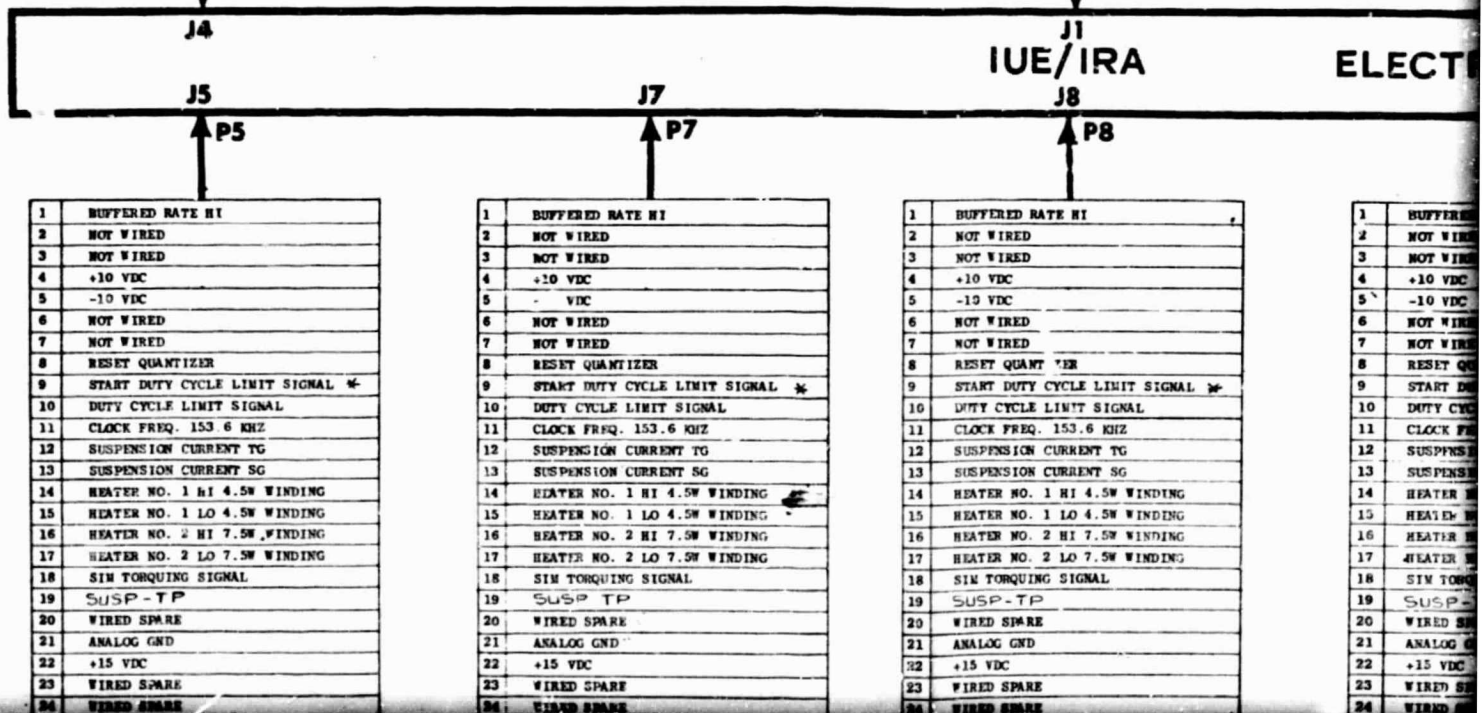
POWER	
1	+28 VDC BUSS 41 HI
2	+28 VDC BUSS 41 HI
3	+28 VDC BUSS 42 HI
4	+28 VDC BUSS 42 HI
5	+28 VDC BUSS 43 HI
6	+28 VDC BUSS 43 HI
7	+28 VDC BUSS 44 HI
8	+28 VDC BUSS 44 HI
9	+28 VDC BUSS 45 HI
10	+28 VDC BUSS 45 HI
11	+28 VDC BUSS 46 HI
12	+28 VDC BUSS 46 HI
13	+28 VDC BUSS 47 HI
14	+28 VDC BUSS 47 HI
15	+28 VDC BUSS 48 HI
16	+28 VDC BUSS 48 HI
17	DC POWER GROUND
18	DC POWER GROUND
19	DC POWER GROUND
20	DC POWER GROUND
21	SPARE
22	SPARE
23	SPARE
24	SPARE
25	SPARE
26	SHIELD

SIGNAL #1	
1	SPARE
2	SPARE
3	SPARE
4	SPARE
5	DATA WORD, COMMON 'A', CD 'A'
6	ENVELOPE, COMMON 'A', CD 'A'
7	SHIFT, COMMON 'A', CD 'A'
8	DATA WORD, COMMON 'B', CD 'A'
9	ENVELOPE, COMMON 'B', CD 'A'
10	SHIFT, COMMON 'B', CD 'A'
11	GYRO 41 HI, DMU 'A'
12	GYRO 42 HI, DMU 'A'
13	GYRO 43 HI, DMU 'A'
14	GYRO 44 HI, DMU 'A'
15	GYRO 45 HI, DMU 'A'
16	GYRO 46 HI, DMU 'A'
17	GYRO 41 ENVELOPE, DMU 'A'
18	GYRO 42 ENVELOPE, DMU 'A'
19	GYRO 43 ENVELOPE, DMU 'A'
20	GYRO 44 ENVELOPE, DMU 'A'
21	GYRO 45 ENVELOPE, DMU 'A'
22	GYRO 46 ENVELOPE, DMU 'A'
23	GYRO 41 SHIFT, DMU 'A'
24	GYRO 42 SHIFT, DMU 'A'
25	GYRO 43 SHIFT, DMU 'A'
26	GYRO 44 SHIFT, DMU 'A'
27	GYRO 45 SHIFT, DMU 'A'
28	GYRO 46 SHIFT, DMU 'A'
29	DMU 'A' INTERROGATE
30	DMU 'A' INTERROGATE
31	STATUS WORD, COM. 'A', DMU 'A'
32	WORD GATE, COM. 'A', DMU 'A'
33	SHIFT, COM. 'A', DMU 'A'
34	STATUS WORD, COM. 'B', DMU 'A'
35	WORD GATE, COM. 'B', DMU 'A'
36	SHIFT, COM. 'B', DMU 'A'
37	LOGIC GROUND
38	LOGIC GROUND
39	BODY RATE, COM. 'A', HI, DMU 'A' T/M
40	BODY RATE, COM. 'A', HI, DMU 'A' T/M
41	BODY RATE, COM. 'A', HI, DMU 'A' T/M
42	BODY RATE, COM. 'A', HI, DMU 'A' T/M
43	BODY RATE, COM. 'A', HI, DMU 'A' T/M
44	BODY RATE, COM. 'A', HI, DMU 'A' T/M
45	BODY RATE, COM. 'A', HI, DMU 'A' T/M

46	GYRO 41 TEMP, DMU 'A' T/M
47	GYRO 43 TEMP, DMU 'A' T/M
48	GYRO 45 TEMP, DMU 'A' T/M
49	ECU TEMP 41, DMU 'A' T/M
50	SPARE
51	GYRO 41 MOTOR CURRENT, DMU 'A' T/M
52	GYRO 43 MOTOR CURRENT, DMU 'A' T/M
53	GYRO 45 MOTOR CURRENT, DMU 'A' T/M
54	ANALOG GROUND
55	ANALOG GROUND
56	GYRO 41 RATE HI, DMU 'A' T/M
57	GYRO 43 RATE HI, DMU 'A' T/M
58	GYRO 45 RATE HI, DMU 'A' T/M
59	BODY RATE, COM. 'A', HI, DMU 'A' T/M
60	BODY RATE, COM. 'A', HI, DMU 'A' T/M
61	BODY RATE, COM. 'A', HI, DMU 'A' T/M
62	GYRO 42 TEMP, DMU 'A' T/M
63	GYRO 44 TEMP, DMU 'A' T/M
64	GYRO 46 TEMP, DMU 'A' T/M
65	GYRO 42 MOTOR CURRENT, DMU 'A' T/M
66	GYRO 44 MOTOR CURRENT, DMU 'A' T/M
67	GYRO 46 MOTOR CURRENT, DMU 'A' T/M
68	GYRO 42 RATE HI, DMU 'A' T/M
69	GYRO 44 RATE HI, DMU 'A' T/M
70	GYRO 46 RATE HI, DMU 'A' T/M
71	BODY RATE, COM. 'B', HI, DMU 'A' T/M
72	BODY RATE, COM. 'B', HI, DMU 'A' T/M
73	SPARE
74	SPARE
75	SPARE
76	SPARE
77	SPARE
78	SHIELD

1	SPARE
2	SPARE
3	SPARE
4	SPARE
5	DATA WORD, COMMON 'A', CD 'A'
6	ENVELOPE, COMMON 'A', CD 'A'
7	SHIFT, COMMON 'A', CD 'A'
8	DATA WORD, COMMON 'B', CD 'A'
9	ENVELOPE, COMMON 'B', CD 'A'
10	SHIFT, COMMON 'B', CD 'A'
11	GYRO 41 HI, DMU 'A'
12	GYRO 42 HI, DMU 'A'
13	GYRO 43 HI, DMU 'A'
14	GYRO 44 HI, DMU 'A'
15	GYRO 45 HI, DMU 'A'
16	GYRO 46 HI, DMU 'A'
17	GYRO 41 ENVELOPE, DMU 'A'
18	GYRO 42 ENVELOPE, DMU 'A'
19	GYRO 43 ENVELOPE, DMU 'A'
20	GYRO 44 ENVELOPE, DMU 'A'
21	GYRO 45 ENVELOPE, DMU 'A'
22	GYRO 46 ENVELOPE, DMU 'A'
23	GYRO 41 SHIFT, DMU 'A'
24	GYRO 42 SHIFT, DMU 'A'
25	GYRO 43 SHIFT, DMU 'A'
26	GYRO 44 SHIFT, DMU 'A'
27	GYRO 45 SHIFT, DMU 'A'
28	GYRO 46 SHIFT, DMU 'A'
29	DMU 'B' INTERROGATE
30	DMU 'B' INTERROGATE
31	STATUS WORD, COM. 'A', DMU 'A'
32	WORD GATE, COM. 'A', DMU 'A'
33	SHIFT, COM. 'A', DMU 'A'
34	STATUS WORD, COM. 'B', DMU 'A'
35	WORD GATE, COM. 'B', DMU 'A'
36	SHIFT, COM. 'B', DMU 'A'
37	LOGIC GROUND
38	LOGIC GROUND
39	BODY RATE, COM. 'A', HI, DMU 'A' T/M
40	BODY RATE, COM. 'A', HI, DMU 'A' T/M
41	BODY RATE, COM. 'A', HI, DMU 'A' T/M
42	BODY RATE, COM. 'A', HI, DMU 'A' T/M
43	BODY RATE, COM. 'A', HI, DMU 'A' T/M
44	BODY RATE, COM. 'A', HI, DMU 'A' T/M
45	BODY RATE, COM. 'A', HI, DMU 'A' T/M

ORIGINAL PAGE IS  
OF POOR QUALITY



SIGNAL #3	
1	WIRE
2	WIRE
3	WIRE
4	WIRE
5	WIRE
6	WIRE
7	WIRE
8	WIRE
9	WIRE
10	WIRE
11	WIRE
12	WIRE
13	WIRE
14	WIRE
15	WIRE
16	WIRE
17	WIRE
18	WIRE
19	WIRE
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190	WIRE
191	WIRE
192	WIRE
193	WIRE
194	WIRE
195	WIRE
196	WIRE
197	WIRE
198	WIRE
199	WIRE
200	WIRE

46	GYRO #1 TEMP. DMU 'B'	T/M
47	GYRO #3 TEMP. DMU 'B'	T/M
48	GYRO #5 TEMP. DMU 'B'	T/M
49	SCU TEMP #1, DMU 'B'	T/M
50	SPARE	
51	GYRO #1 MOTOR CURRENT. DMU 'B'	T/M
52	GYRO #3 MOTOR CURRENT. DMU 'B'	T/M
53	GYRO #5 MOTOR CURRENT. DMU 'B'	T/M
54	ANALOG GROUND	
55	ANALOG GROUND	
56	GYRO #1 RATE HI. DMU 'B'	T/M
57	GYRO #3 RATE HI. DMU 'B'	T/M
58	GYRO #5 RATE HI. DMU 'B'	T/M
59	BODY RATE, COM 'B' $\omega_c$ RETURN	
60	BODY RATE, COM 'B' $\omega_c$ RETURN	
61	BODY RATE, COM 'B' $\omega_c$ HI. DMU 'B' T/M	
62	GYRO #2 TEMP. DMU 'B'	T/M
63	GYRO #4 TEMP. DMU 'B'	T/M
64	GYRO #6 TEMP. DMU 'B'	T/M
65	GYRO #2 MOTOR CURRENT. DMU 'B'	T/M
66	GYRO #4 MOTOR CURRENT. DMU 'B'	T/M
67	GYRO #6 MOTOR CURRENT. DMU 'B'	T/M
68	GYRO #2 RATE HI. DMU 'B'	T/M
69	GYRO #4 RATE HI. DMU 'B'	T/M
70	GYRO #6 RATE HI. DMU 'B'	T/M
71	BODY RATE, COM 'B' $\omega_c$ HI. DMU 'B' T/M	
72	BODY RATE, COM 'B' $\omega_c$ HI. DMU 'B' T/M	
73	SPARE	
74	SPARE	
75	SPARE	
76	SPARE	
77	SPARE	
78	SHIELD	

1	-15 VDC, GYRO #1
2	-10 VDC, GYRO #1
3	-10 VDC, GYRO #1
4	+5 VDC, GYRO #1
5	-15 VDC, GYRO #2
6	-10 VDC, GYRO #2
7	-10 VDC, GYRO #2
8	+5 VDC, GYRO #2
9	-15 VDC, GYRO #3
10	+10 VDC, GYRO #3
11	-10 VDC, GYRO #3
12	+5 VDC, GYRO #3
13	-15 VDC, GYRO #4
14	-10 VDC, GYRO #4
15	-10 VDC, GYRO #4
16	+5 VDC, GYRO #4
17	-15 VDC, GYRO #5
18	-10 VDC, GYRO #5
19	-10 VDC, GYRO #5
20	+5 VDC, GYRO #5
21	-15 VDC, GYRO #6
22	+10 VDC, GYRO #6
23	-10 VDC, GYRO #6
24	+5 VDC, GYRO #6
25	SPARE
26	SIM. TORQ. SIG. GYRO #1
27	SIM. TORQ. SIG. GYRO #2
28	SIM. TORQ. SIG. GYRO #3
29	SIM. TORQ. SIG. GYRO #4
30	SIM. TORQ. SIG. GYRO #5
31	SIM. TORQ. SIG. GYRO #6
32	MICROSYN EXC. GYRO #1 HI
33	MICROSYN EXC. GYRO #2 HI
34	MICROSYN EXC. GYRO #3 HI
35	MICROSYN EXC. GYRO #4 HI
36	MICROSYN EXC. GYRO #5 HI
37	MICROSYN EXC. GYRO #6 HI
38	SIM TORQ TEST 1,3,5
39	SIM TORQ TEST 2,4,6
40	WHL ENT TEST 1,3,5
41	WHL ENT TEST 2,4,6
42	SPARE
43	SPARE
44	GYRO #1 HTR DUTY CYCLE HI
45	GYRO #2 HTR DUTY CYCLE HI
46	GYRO #3 HTR DUTY CYCLE HI
47	GYRO #4 HTR DUTY CYCLE HI
48	GYRO #5 HTR DUTY CYCLE HI
49	GYRO #6 HTR DUTY CYCLE HI
50	HTR DUTY CYCLE GND
51	SUS CNT 1,3,5
52	SUS CNT 2,4,6
53	SPARE
54	SPARE
55	SPARE
56	GYRO #1 WHEEL VOLTS #A LO

57	GYRO #1 WHEEL VOLTS #A LO
58	GYRO #2 WHEEL VOLTS #A HI
59	GYRO #2 WHEEL VOLTS #A LO
60	GYRO #3 WHEEL VOLTS #A HI
61	GYRO #3 WHEEL VOLTS #A LO
62	GYRO #4 WHEEL VOLTS #A HI
63	GYRO #4 WHEEL VOLTS #A LO
64	GYRO #5 WHEEL VOLTS #A HI
65	GYRO #5 WHEEL VOLTS #A LO
66	GYRO #6 WHEEL VOLTS #A HI
67	GYRO #6 WHEEL VOLTS #A LO
68	SPARE
69	SUSP. EXC. GYRO #1 HI
70	SUSP. EXC. GYRO #2 HI
71	SUSP. EXC. GYRO #3 HI
72	SUSP. EXC. GYRO #4 HI
73	SUSP. EXC. GYRO #5 HI
74	SUSP. EXC. GYRO #6 HI
75	SUSP. CURR. GYRO #1 TO LO
76	SUSP. CURR. GYRO #1 SG LO
77	SUSP. CURR. GYRO #2 TO LO
78	SUSP. CURR. GYRO #2 SG LO
79	SUSP. CURR. GYRO #3 TO LO
80	SUSP. CURR. GYRO #3 SG LO
81	SUSP. CURR. GYRO #4 TO LO
82	SUSP. CURR. GYRO #4 SG LO
83	SUSP. CURR. GYRO #5 TO LO
84	SUSP. CURR. GYRO #5 SG LO
85	SUSP. CURR. GYRO #6 TO LO
86	SUSP. CURR. GYRO #6 SG LO
87	BUFF. RATE, GYRO #1 HI
88	BUFF. RATE, GYRO #2 HI
89	BUFF. RATE, GYRO #3 HI
90	BUFF. RATE, GYRO #4 HI
91	BUFF. RATE, GYRO #5 HI
92	BUFF. RATE, GYRO #6 HI
93	307.2 KHZ COM. 'A'
94	307.2 KHZ COM. 'B'
95	DETO COM. 'A'
96	DETO COM. 'B'
97	GYRO #1 QUANTIZER OUTPUT
98	GYRO #2 QUANTIZER OUTPUT
99	GYRO #3 QUANTIZER OUTPUT
100	GYRO #4 QUANTIZER OUTPUT
101	GYRO #5 QUANTIZER OUTPUT
102	GYRO #6 QUANTIZER OUTPUT
103	SIGNAL GROUND
104	SHIELD

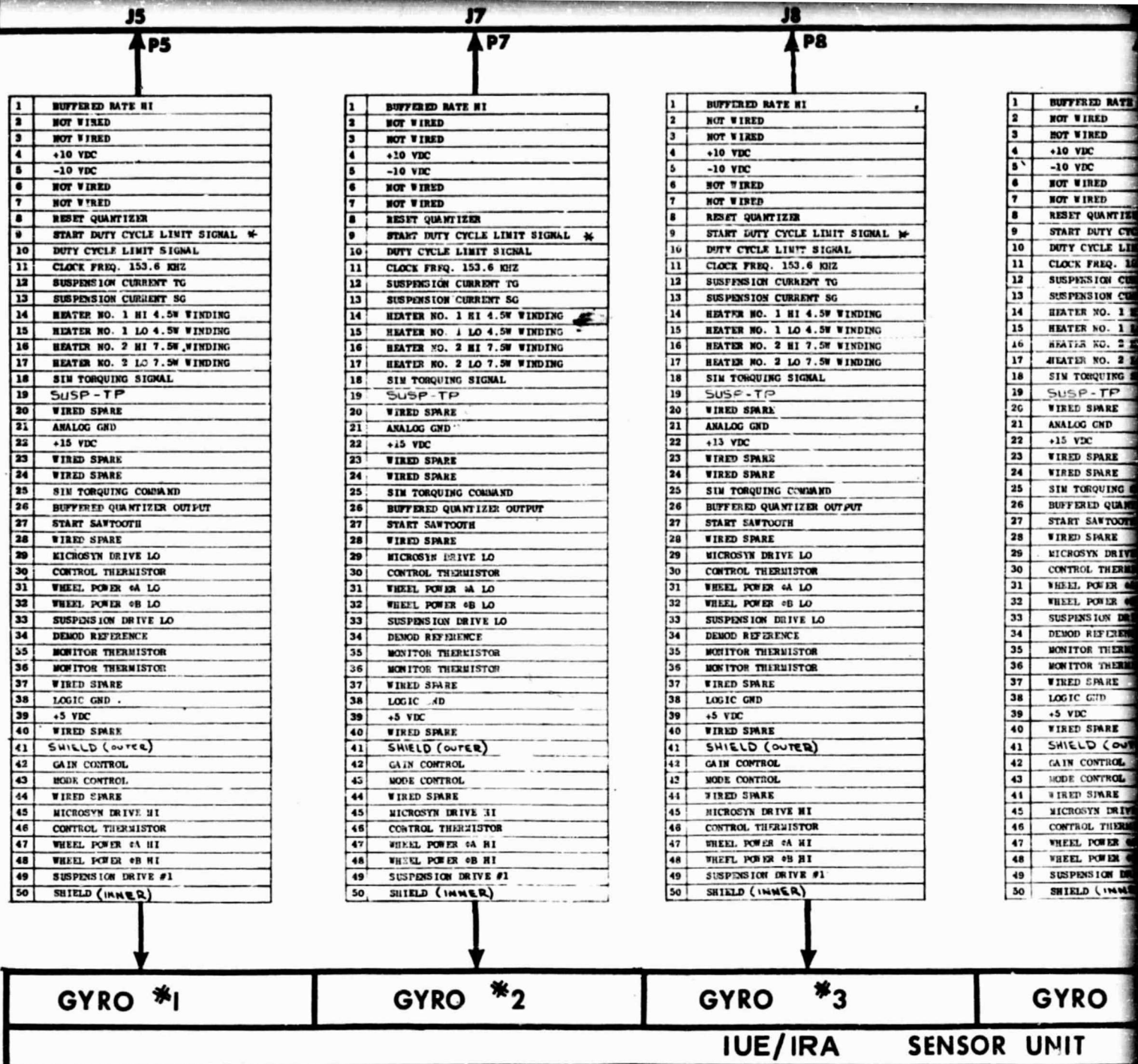
## ELECTRONIC CONTROL UNIT

J9	P9
1	BUFFERED RATE HI
2	NOT WIRED
3	NOT WIRED
4	+10 VDC
5	-10 VDC
6	NOT WIRED
7	NOT WIRED
8	RESET QUANTIZER
9	START DUTY CYCLE LIMIT SIGNAL *
10	DUTY CYCLE LIMIT SIGNAL
11	CLOCK FREQ. 153.6 KHZ
12	SUSPENSION CURRENT TG
13	SUSPENSION CURRENT SG
14	HEATER NO. 1 HI 4.5W WINDING
15	HEATER NO. 1 LO 4.5W WINDING
16	HEATER NO. 2 HI 7.5W WINDING
17	HEATER NO. 2 LO 7.5W WINDING
18	SIM TORQUING SIGNAL
19	SUSP-TP
20	WIRED SPARE
21	ANALOG GND
22	+15 VDC
23	WIRED SPARE
24	WIRED SPARE

J6	P6
1	BUFFERED RATE HI
2	NOT WIRED
3	NOT WIRED
4	+10 VDC
5	-10 VDC
6	NOT WIRED
7	NOT WIRED
8	RESET QUANTIZER
9	START DUTY CYCLE LIMIT SIGNAL *
10	DUTY CYCLE LIMIT SIGNAL
11	CLOCK FREQ. 153.6 KHZ
12	SUSPENSION CURRENT TG
13	SUSPENSION CURRENT SG
14	HEATER NO. 1 HI 4.5W WINDING
15	HEATER NO. 1 LO 4.5W WINDING
16	HEATER NO. 2 HI 7.5W WINDING
17	HEATER NO. 2 LO 7.5W WINDING
18	SIM TORQUING SIGNAL
19	SUSP-TP
20	WIRED SPARE
21	ANALOG GND
22	+15 VDC
23	WIRED SPARE
24	WIRED SPARE

J10	P10
1	BUFFERED RATE HI
2	NOT WIRED
3	NOT WIRED
4	+10 VDC
5	-10 VDC
6	NOT WIRED
7	NOT WIRED
8	RESET QUANTIZER
9	START DUTY CYCLE LIMIT SIGNAL *
10	DUTY CYCLE LIMIT SIGNAL
11	CLOCK FREQ. 153.6 KHZ
12	SUSPENSION CURRENT TG
13	SUSPENSION CURRENT SG
14	HEATER NO. 1 HI 4.5W WINDING
15	HEATER NO. 1 LO 4.5W WINDING
16	HEATER NO. 2 HI 7.5W WINDING
17	HEATER NO. 2 LO 7.5W WINDING
18	SIM TORQUING SIGNAL
19	SUSP-TP
20	WIRED SPARE
21	ANALOG GND
22	+15 VDC
23	WIRED SPARE
24	WIRED SPARE

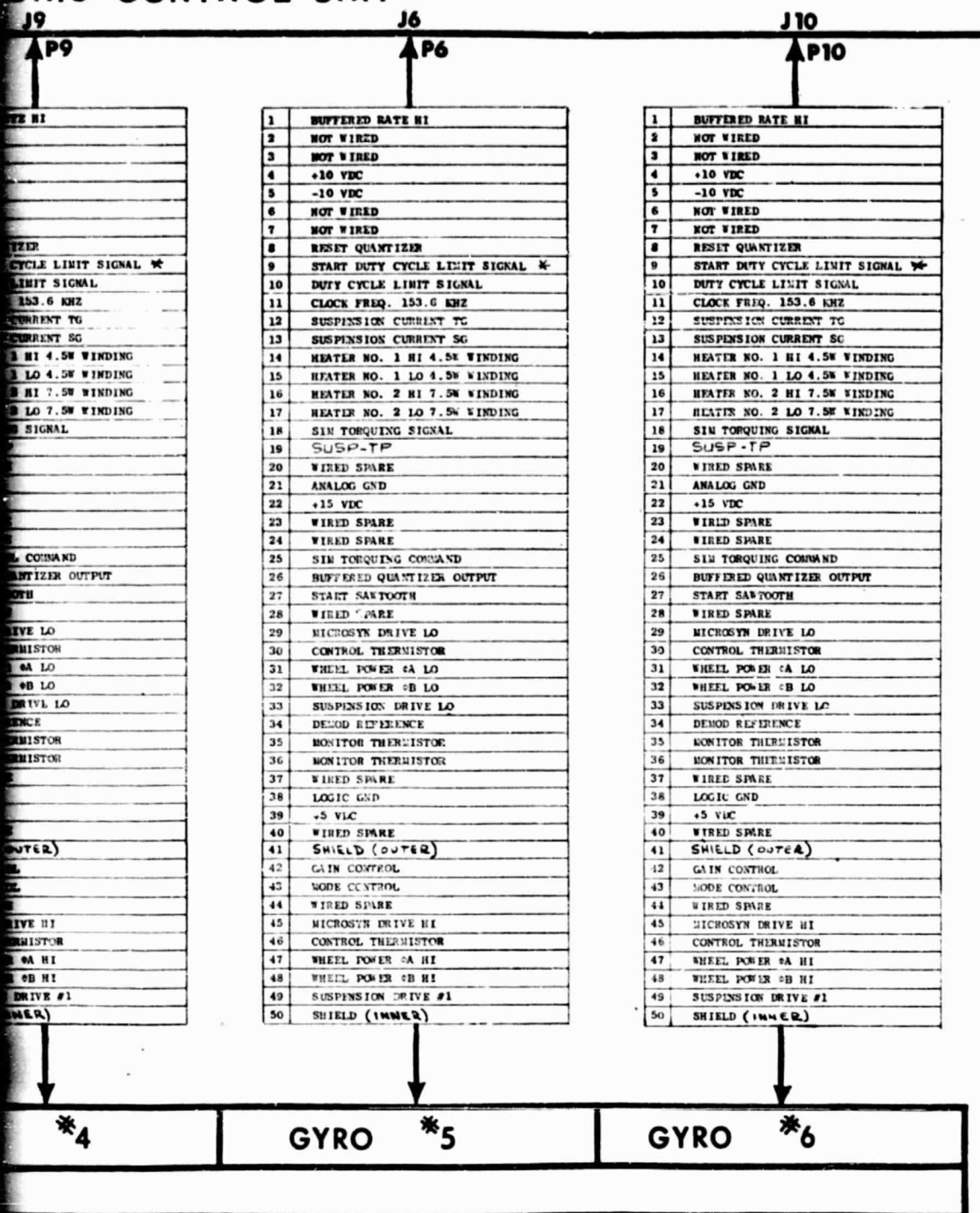
REVISIONS			
LTR	DESCRIPTION	DATE	APP
A	REVISED	6-17-73	HB
B	REVISED CRYSTAL 1	6-17-73	HB
C	CRYSTAL 1 REFE	6-17-73	HB



WELDOUT FRAME



# ONIC CONTROL UNIT



REVISIONS			
LTR	DESCRIPTION	DATE	APPD
A	REVISED	6-17-75	MB
B	REVISED CRYSTAL	6-11-76	MB
C	REVISED REF	8-21-77	MB

**NOTES**

J<sub>1</sub> - 311 P 407-55-B-15 MATES WITH 311 P 407-5P-B-15

J<sub>2</sub> - 311 P 407-65-B-15 MATES WITH - 311 P 407-6P-B-15

J<sub>3</sub> - 311 P 407-55-B-15 MATES WITH - 311 P 407-5P-B-15

J<sub>4</sub> - 311 P 407-2P-B-15 MATES WITH - 311 P 407-2S-B-15

P<sub>5</sub> - P<sub>10</sub> - CANNON EDWARDSOP (NIL N 24308/3-5) ALL KEYS

J<sub>5</sub> - J<sub>10</sub> - CANNON EDWARDSOP (NIL N 24308/2-5) ALL KEYS TO P<sub>5</sub>-P<sub>10</sub>

**Bendix** GUIDANCE SYSTEMS DIVISION

THE BENDIX CORPORATION NAVIGATION & CONTROL DIVISION TETERBORO, NEW JERSEY, U.S.A.

IUE/IRA PIN FUNCTION DIAGRAM

SIZE CODE IDENT NO. 5114038  
E 19315

FOLDOUT FRAME

Issue: Rev. B

Date: 20 January 1975

DETAILED ELECTRICAL

FUNCTION	CONNECTOR	PIN#	INPUT	OUTPUT	Z <sub>S</sub> or Z <sub>L</sub>	CH
+28 VDC BUSS #1 HI	POWER (J4)	1	X		R= $\Omega$	
+28 VDC BUSS #1 HI	"	2	X		R= $\Omega$	
+28 VDC BUSS #2 HI	"	3	X		R= $\Omega$	
+28 VDC BUSS #2 HI	"	4	X		R= $\Omega$	
+28 VDC BUSS #3 HI	"	5	X		R= $\Omega$	
+28 VDC BUSS #3 HI	"	6	X		R= $\Omega$	
+28 VDC BUSS #4 HI	"	7	X	62.2	R= $\Omega$	
+28 VDC BUSS #4 HI	"	8	X	$\Omega$	R= $\Omega$	
+28 VDC BUSS #5 HI	"	9	X		R= $\Omega$	
+28 VDC BUSS #5 HI	"	10	X		R= $\Omega$	
+28 VDC BUSS #6 HI	"	11	X		R= $\Omega$	
+28 VDC BUSS #6 HI	"	12	X		R= $\Omega$	
+28 VDC BUSS #7 HI	"	13	X		R= $\Omega$	
+28 VDC BUSS #7 HI	"	14	X		R= $\Omega$	
+28 VDC BUSS #8 HI	"	15	X	509	R= $\Omega$	
+28 VDC BUSS #8 HI	"	16	X	$\Omega$	R= $\Omega$	
DC POWER GROUND	"	17	X			
DC POWER GROUND	"	18	X			
DC POWER GROUND	"	19	X			
DC POWER GROUND	"	20	X			
SPARE	"	21				
SPARE	"	22				
SPARE	"	23				
SPARE	"	24				
SPARE	"	25				
SHIELD	"	26				
SPARE	SIGNAL #1	1				
SPARE	" (J1)	2				
SPARE	"	3				
SPARE	"	4				
DATA WORD, COMMON 'A', CD 'A'	"	5	X		100K $\Omega$	
ENVELOPE, COMMON 'A', CD 'A'	"	6	X		100K $\Omega$	
SHIFT, COMMON 'A', CD 'A'	"	7	X		100K $\Omega$	
DATA WORD, COMMON 'B', CD 'A'	"	8	X		100K $\Omega$	
ENVELOPE, COMMON 'B', CD 'A'	"	9	X		100K $\Omega$	
SHIFT, COMMON 'B', CD 'A'	"	10	X		100K $\Omega$	
GYRO #1 $\Delta\theta$ , DMU 'A'	"	11		X	1K $\Omega$	
GYRO #2 $\Delta\theta$ , DMU 'A'	"	12		X	1K $\Omega$	

FOLDOUT

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FOLDOUT FRAME

Issue: Rev. B

Date: 20 January 1975

DETAILED ELECTRICAL  
(CONTINUED)

FUNCTION	CONNECTOR	PIN#	INPUT	OUTPUT	Z <sub>S</sub> or Z <sub>L</sub>	CKT
GYRO #3 $\Delta\theta$ , DMU 'A'	SIGNAL #1	13		X	1K $\Omega$	DO-
GYRO #4 $\Delta\theta$ , DMU 'A'	" (J1)	14		X	1K $\Omega$	DO-
GYRO #5 $\Delta\theta$ , DMU 'A'	"	15		X	1K $\Omega$	DO-
GYRO #6 $\Delta\theta$ , DMU 'A'	"	16		X	1K $\Omega$	DO-
GYRO #1 ENVELOPE, DMU 'A'	"	17	X		100K $\Omega$	DI-
GYRO #2 ENVELOPE, DMU 'A'	"	18	X		100K $\Omega$	DI-
GYRO #3 ENVELOPE, DMU 'A'	"	19	X		100K $\Omega$	DI-
GYRO #4 ENVELOPE, DMU 'A'	"	20	X		100K $\Omega$	DI-
GYRO #5 ENVELOPE, DMU 'A'	"	21	X		100K $\Omega$	DI-
GYRO #6 ENVELOPE, DMU 'A'	"	22	X		100K $\Omega$	DI-
GYRO #1 SHIFT, DMU 'A'	"	23	X		100K $\Omega$	DI-
GYRO #2 SHIFT, DMU 'A'	"	24	X		100K $\Omega$	DI-
GYRO #3 SHIFT, DMU 'A'	"	25	X		100K $\Omega$	DI-
GYRO #4 SHIFT, DMU 'A'	"	26	X		100K $\Omega$	DI-
GYRO #5 SHIFT, DMU 'A'	"	27	X		100K $\Omega$	DI-
GYRO #6 SHIFT, DMU 'A'	"	28	X		100K $\Omega$	DI-
DMU 'A', INTERROGATE	"	29	X		3.3K $\Omega$	DI-
DMU 'A', INTERROGATE	"	30	X		3.3K $\Omega$	DI-
STATUS WORD, COM. 'A', DMU 'A'	"	31			511 $\Omega$	DO-
WORD GATE, COM. 'A', DMU 'A'	"	32	X		3.3K $\Omega$	DI-
SHIFT, COM. 'A', DMU 'A'	"	33	X		2.2K $\Omega$	DI-
STATUS WORD, COM. 'B', DMU 'A'	"	34		X	511 $\Omega$	DO-
WORD GATE, COM. 'B', DMU 'A'	"	35	X		3.3K $\Omega$	DI-
SHIFT, COM. 'B', DMU 'A'	"	36	X		2.2K $\Omega$	DI-
LOGIC GROUND	"	37				
LOGIC GROUND	"	38				
BODY RATE, COM. 'A' $\omega_{zc}$ HI	"	39		X	1K $\Omega$	AO-
BODY RATE, COM. 'A' $\omega_{yc}$ HI	"	40		X	1K $\Omega$	AO-
BODY RATE, COM. 'A' $\omega_{xc}$ HI	"	41		X	1K $\Omega$	AO-
BODY RATE, COM. 'A' GROUND	"	42				
BODY RATE, COM. 'A' $\omega_{zc}$ HI, DMU 'A', T/M	"	43		X	4.99K $\Omega$	AO-
BODY RATE, COM. 'A' $\omega_{yc}$ HI, DMU 'A', T/M	"	44		X	4.99K $\Omega$	AO-
BODY RATE, COM. 'A' $\omega_{xc}$ HI, DMU 'A', T/M	"	45		X	4.99K $\Omega$	AO-
GYRO #1 TEMP, DMU 'A' T/M	"	46		X	4.99K $\Omega$	AO-
GYRO #3 TEMP, DMU 'A' T/M	"	47		X	4.99K $\Omega$	AO-
GYRO #5 TEMP, DMU 'A' T/M	"	48		X	4.99K $\Omega$	AO-
ECU TEMP #1, DMU 'A' T/M	"	49		X	VARIABLE	
ECU TEMP #2, DMU 'A' T/M	"	50		X	VARIABLE	

REDACTED



DETAILED ELECTRICAL INTERFACE  
(CONTINUED)

OUTPUT	Z <sub>S</sub> or Z <sub>L</sub>	CKT. TYPE	VOLT. RANGE	REMARKS
X	1K $\Omega$	DO-1	LOGIC LEVEL	"1" = 3.5-5.5 VDC. "0" = 0-0.4 VDC
X	1K $\Omega$	DO-1	"	"
X	1K $\Omega$	DO-1	"	"
X	1K $\Omega$	DO-1	"	"
	100K $\Omega$	DI-1	"	"1" = 3.5-10 VDC. "0" = 0-1.5 VDC
	100K $\Omega$	DI-1	"	"
	100K $\Omega$	DI-1	"	"
	100K $\Omega$	DI-1	"	"
	100K $\Omega$	DI-1	"	"
	100K $\Omega$	DI-1	"	"
	100K $\Omega$	DI-1	"	"
	100K $\Omega$	DI-1	"	"
	100K $\Omega$	DI-1	"	"
	100K $\Omega$	DI-1	"	"
	100K $\Omega$	DI-1	"	"
	100K $\Omega$	DI-1	"	"
	100K $\Omega$	DI-1	"	"
	3.3K $\Omega$	DI-1	"	"
	3.3K $\Omega$	DI-1	"	"
	511 $\Omega$	DO-1	"	"1" = 3.5-5.5 VDC. "0" = 0-0.4 VDC
	3.3K $\Omega$	DI-2	"	
	2.2K $\Omega$	DI-3	"	
X	511 $\Omega$	DO-1	"	"1" = 3.5-5.5 VDC. "0" = 0-0.4 VDC
	3.3K $\Omega$	DI-2	"	
	2.2K $\Omega$	DI-3	"	
X	1K $\Omega$	AO-1	$\pm$ 5VDC. 22 ma	SHIELD EXTERNAL TO IRA. 1V/ $^{\circ}$ SEC. 0.05V/SEC/SEC
X	1K $\Omega$	AO-1	$\pm$ 5VDC. 22 ma	SHIELD EXTERNAL TO IRA. 1V/ $^{\circ}$ SEC. 0.05V/SEC/SEC
X	1K $\Omega$	AO-1	$\pm$ 5VDC. 22ma	SHIELD EXTERNAL TO IRA. 1V/ $^{\circ}$ SEC. 0.05V/SEC/SEC
X	4.99K $\Omega$	AO-2	-0.7 TO +5.6VDC	$\pm$ 100 SEC/SEC OR $\pm$ 5 $^{\circ}$ /SEC RANGE = 0-5VDC
X	4.99K $\Omega$	AO-2	"	+100 SEC/SEC OR + 5 $^{\circ}$ /SEC RANGE = 0-5VDC
X	4.99K $\Omega$	AO-2	"	$\pm$ 100 SEC/SEC OR $\pm$ 5 $^{\circ}$ /SEC RANGE = 0-5VDC
X	4.99K $\Omega$	AO-2	"	27 mv/ $^{\circ}$ F. 135 $^{\circ}$ F = 3 VOLTS DC
X	4.99K $\Omega$	AO-2	"	27 mv/ $^{\circ}$ F. 135 $^{\circ}$ F = 3 VOLTS DC
X	4.99K $\Omega$	AO-2	"	27 mv/ $^{\circ}$ F. 135 $^{\circ}$ F = 3 VOLTS DC
X	VARIABLE		RESISTANCE	YSI THERMISTOR. ONE SIDE GND'ED
X	VARIABLE		RESISTANCE	YSI THERMISTOR. ONE SIDE GND'ED

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DETAILED ELECTRICAL  
(CONTINUED)

FUNCTION	CONNECTOR	PIN#	INPUT	OUTPUT	Z <sub>S</sub> or Z <sub>L</sub>	CKT
GYRO #1 $\Phi$ B MOTOR CURRENT, DMU 'A', T/M	SIGNAL #1	51		X	4.99K $\Omega$	AO
GYRO #3 $\Phi$ B MOTOR CURRENT, DMU 'A', T/M	" (J1)	52		X	4.99K $\Omega$	AO
GYRO #5 $\Phi$ B MOTOR CURRENT, DMU 'A', T/M	"	53		X	4.99K $\Omega$	AO
ANALOG GROUND	"	54				
ANALOG GROUND	"	55				
GYRO #1 RATE HI, DMU 'A', T/M	"	56		X	4.99K $\Omega$	AO
GYRO #3 RATE HI, DMU 'A', T/M	"	57		X	4.99K $\Omega$	AO
GYRO #5 RATE HI, DMU 'A', T/M	"	58		X	4.99K $\Omega$	AO
BODY RATE.COM. 'B' $\omega$ zc HI, DMU 'A' T/M	"	59		X	4.99K $\Omega$	AO
BODY RATE.COM. 'E' $\omega$ vc HI, DMU 'A' T/M	"	60		X	4.99K $\Omega$	AO
BODY RATE.COM. 'B' $\omega$ xc HI, DMU 'A' T/M	"	61		X	4.99K $\Omega$	AO
GYRO #2 TEMP, DMU 'A' T/M	"	62		X	4.99K $\Omega$	AO
GYRO #4 TEMP, DMU 'A' T/M	"	63		X	4.99K $\Omega$	AO
GYRO #6 TEMP, DMU 'A' T/M	"	64		X	4.99K $\Omega$	AO
GYRO #2 $\Phi$ B MOTOR CURRENT, DMU 'A' T/M	"	65		X	4.99K $\Omega$	AO
GYRO #4 $\Phi$ B MOTOR CURRENT, DMU 'A' T/M	"	66		X	4.99K $\Omega$	AO
GYRO #6 $\Phi$ B MOTOR CURRENT, DMU 'A' T/M	"	67		X	4.99K $\Omega$	AO
GYRO #2 RATE HI, DMU 'A' T/M	"	68		X	4.99K $\Omega$	AO
GYRO #4 RATE HI, DMU 'A' T/M	"	69		X	4.99K $\Omega$	AO
GYRO #6 RATE HI, DMU 'A' T/M	"	70		X	4.99K $\Omega$	AO
SPARE	"	71				
SPARE	"	72				
SPARE	"	73				
SPARE	"	74				
SPARE	"	75				
SPARE	"	76				
SPARE	"	77				
SHIELD	"	78				
SPARE	SIGNAL #2	1				
SPARE	" (J3)	2				
SPARE	"	3				
SPARE	"	4				
DATA WORD, COMMON 'A', CD 'B'	"	5	X		100K $\Omega$	DI
ENVELOPE, COMMON 'A', CD 'B'	"	6	X		100K $\Omega$	DI
SHIFT, COMMON 'A', CD 'B'	"	7	X		100K $\Omega$	DI
DATA WORD, COMMON 'B', CD 'B'	"	8	X		100K $\Omega$	DI
ENVELOPE, COMMON 'B', CD 'B'	"	9	X		100K $\Omega$	DI
SHIFT, COMMON 'B', CD 'B'	"	10	X		100K $\Omega$	DI

FOLDOUT FRAME

DETAILED ELECTRICAL INTERFACE  
(CONTINUED)

OUTPUT	$Z_S$ or $Z_L$	CKT. TYPE	VOLT. RANGE	REMARKS
X	4.99K $\Omega$	AO-2	-0.7 TO +5.6VDC	0-5 VDC = 0 TO 600 ma GYRO CURRENT
X	4.99K $\Omega$	AO-2	"	"
X	4.99K $\Omega$	AO-2	"	"
X	4.99K $\Omega$	AO-2	-0.7 TO +5.6VDC	0-5 VDC = $\pm 600 \text{ SEC/SEC}$ OR $\pm 5^\circ/\text{SEC}$
X	4.99K $\Omega$	AO-2	"	"
X	4.99K $\Omega$	AO-2	"	"
X	4.99K $\Omega$	AO-2	"	$\pm 100 \text{ SEC/SEC}$ OR $\pm 5^\circ/\text{SEC}$ = 0-5 VDC
X	4.99K $\Omega$	AO-2	"	"
X	4.99K $\Omega$	AO-2	"	"
X	4.99K $\Omega$	AO-2	"	27 mv/ $^\circ\text{F}$ , 135 $^\circ\text{F}$ = 3 VOLTS DC
X	4.99K $\Omega$	AO-2	"	"
X	4.99K $\Omega$	AO-2	"	"
X	4.99K $\Omega$	AO-2	"	0-5 VDC = 0 TO 600 ma GYRO CURRENT
X	4.99K $\Omega$	AO-2	"	"
X	4.99K $\Omega$	AO-2	"	"
X	4.99K $\Omega$	AO-2	"	0-5 VDC = $\pm 600 \text{ SEC/SEC}$ OR $\pm 5^\circ/\text{SEC}$
X	4.99K $\Omega$	AO-2	"	"
X	4.99K $\Omega$	AO-2	"	"
				(NOTE) - FOR ALL REMARKS ON SIGNAL #2
				CONNECTOR SEE CORRESPONDING SIGNAL #1
				PIN NUMBER
	100K $\Omega$	DI-1	LOGIC LEVEL	
	100K $\Omega$	DI-1	"	
	100K $\Omega$	DI-1	"	
	100K $\Omega$	DI-1	"	
	100K $\Omega$	DI-1	"	
	100K $\Omega$	DI-1	"	

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DETAILED ELECTRICAL  
(CONTINUED)

FUNCTION	CONNECTOR	PIN#	INPUT	OUTPUT	Z <sub>S</sub> or Z <sub>L</sub>	CKT
GYRO #1 $\Delta\theta$ , DMU 'B'	SIGNAL #2	11		X	1K $\Omega$	
GYRO #2 $\Delta\theta$ , DMU 'B'	" (J3)	12		X	1K $\Omega$	
GYRO #3 $\Delta\theta$ , DMU 'B'	"	13		X	1K $\Omega$	
GYRO #4 $\Delta\theta$ , DMU 'B'	"	14		X	1K $\Omega$	
GYRO #5 $\Delta\theta$ , DMU 'B'	"	15		X	1K $\Omega$	
GYRO #6 $\Delta\theta$ , DMU 'B'	"	16		X	1K $\Omega$	
GYRO #1 ENVELOPE, DMU 'B'	"	17	X		100K $\Omega$	
GYRO #2 ENVELOPE, DMU 'B'	"	18	X		100K $\Omega$	
GYRO #3 ENVELOPE, DMU 'B'	"	19	X		100K $\Omega$	
GYRO #4 ENVELOPE, DMU 'B'	"	20	X		100K $\Omega$	
GYRO #5 ENVELOPE, DMU 'B'	"	21	X		100K $\Omega$	
GYRO #6 ENVELOPE, DMU 'B'	"	22	X		100K $\Omega$	
GYRO #1 SHIFT, DMU 'B'	"	23	X		100K $\Omega$	
GYRO #2 SHIFT, DMU 'B'	"	24	X		100K $\Omega$	
GYRO #3 SHIFT, DMU 'B'	"	25	X		100K $\Omega$	
GYRO #4 SHIFT, DMU 'B'	"	26	X		100K $\Omega$	
GYRO #5 SHIFT, DMU 'B'	"	27	X		100K $\Omega$	
GYRO #6 SHIFT, DMU 'B'	"	28	X		100K $\Omega$	
DMU 'B' INTERROGATE	"	29	X		3.3K $\Omega$	
DMU 'B' INTERROGATE	"	30	X		3.3K $\Omega$	
STATUS WORD, COM. 'A', DMU 'B'	"	31			511 $\Omega$	
WORD GATE, COM. 'A', DMU 'B'	"	32	X		3.3K $\Omega$	
SHIFT, COM. 'A', DMU 'B'	"	33	X		2.2K $\Omega$	
STATUS WORD, COM. 'B', DMU 'B'	"	34			511 $\Omega$	
WORD GATE, COM. 'B', DMU 'B'	"	35	X		3.3K $\Omega$	
SHIFT, COM. 'B', DMU 'B'	"	36	X		2.2K $\Omega$	
LOGIC GROUND	"	37				
LOGIC GROUND	"	38				
BODY RATE, COM. 'B' $\omega_{zc}$ HI	"	39		X	1K $\Omega$	
BODY RATE, COM. 'B' $\omega_{yc}$ HI	"	40		X	1K $\Omega$	
BODY RATE, COM. 'B' $\omega_{xc}$ HI	"	41		X	1K $\Omega$	
BODY RATE, COM. 'B' GROUND	"	42				
BODY RATE, COM. 'A' $\omega_{zc}$ HI, DMU 'B', T/M	"	43		X		
BODY RATE, COM. 'A' $\omega_{yc}$ HI, DMU 'B', T/M	"	44		X		
BODY RATE, COM. 'A' $\omega_{xc}$ HI, DMU 'B', T/M	"	45		X		

FOLDOUT FRAME



DETAILED ELECTRICAL INTERFACE  
(CONTINUED)

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OUTPUT	Z <sub>S</sub> or Z <sub>L</sub>	CKT. TYPE	VOLT. RANGE	REMARKS
X	1K $\Omega$	DO-1	LOGIC LEVEL	NOTE - FOR ALL REMARKS ON SIGNAL #2
X	1K $\Omega$	DO-1	"	CONNECTOR SEE CORRESPONDING SIGNAL #1
X	1K $\Omega$	DO-1	"	PIN NUMBER
X	1K $\Omega$	DO-1	"	
X	1K $\Omega$	DO-1	"	
X	1K $\Omega$	DO-1	"	
	100K $\Omega$	DI-1	"	
	100K $\Omega$	DI-1	"	
	100K $\Omega$	DI-1	"	
	100K $\Omega$	DI-1	"	
	100K $\Omega$	DI-1	"	
	100K $\Omega$	DI-1	"	
	100K $\Omega$	DI-1	"	
	100K $\Omega$	DI-1	"	
	100K $\Omega$	DI-1	"	
	100K $\Omega$	DI-1	"	
	100K $\Omega$	DI-1	"	
	100K $\Omega$	DI-1	"	
	100K $\Omega$	DI-1	"	
	100K $\Omega$	DI-1	"	
	100K $\Omega$	DI-1	"	
	3.3K $\Omega$	DI-1	"	
	3.3K $\Omega$	DI-1	"	
	511 $\Omega$	DO-1	"	
	3.3K $\Omega$	DI-2	"	
	2.2K $\Omega$	DI-3	"	
	511 $\Omega$	DO-1	"	
	3.3K $\Omega$	DI-2	"	
	2.2K $\Omega$	DI-3	"	
X	1K $\Omega$	AO-1	$\pm$ 5VDC 22 MA	
X	1K $\Omega$	AO-1	$\pm$ 5VDC 22 MA	
X	1K $\Omega$	AO-1	$\pm$ 5VDC 22 MA	
X		AO-2	-0.7 TO +5.6VDC	
X		AO-2	"	
X		AO-2	"	

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DETAILED ELECTRICAL  
(CONTINUED)

FUNCTION	CONNECTOR	PIN#	INPUT	OUTPUT	Z <sub>S</sub> or Z <sub>L</sub>	CKT
GYRO #1 TEMP. DMU 'B' T/M	SIGNAL #2	46		X	4.99K $\Omega$	AC
GYRO #3 TEMP. DMU 'B' T/M	" (J3)	47		X	4.99K $\Omega$	AC
GYRO #5 TEMP. DMU 'B' T/M	"	48		X	4.99K $\Omega$	AC
ECU TEMP #1. DMU 'B' T/M	"	49		X	VARIABLE	
ECU TEMP #2. DMU 'B' T/M	"	50		X	VARIABLE	
GYRO #1 $\phi$ B MOTOR CURRENT, DMU 'B' T/M	"	51		X	4.99K $\Omega$	AC
GYRO #3 $\phi$ B MOTOR CURRENT, DMU 'B' T/M	"	52		X	4.99K $\Omega$	AC
GYRO #5 $\phi$ B MOTOR CURRENT, DMU 'B' T/M	"	53		X	4.99K $\Omega$	AC
ANALOG GROUND	"	54				
ANALOG GROUND	"	55				
GYRO #1 RATE HI. DMU 'B' T/M	"	56		X	4.99K $\Omega$	AC
GYRO #3 RATE HI. DMU 'B' T/M	"	57		X	4.99K $\Omega$	AC
GYRO #5 RATE HI. DMU 'B' T/M	"	58		X	4.99K $\Omega$	AC
BODY RATE, COM. 'B' $\omega$ zc HI, DMU 'B' T/M	"	59		X	4.99K $\Omega$	AC
BODY RATE, COM. 'B' $\omega$ yc HI, DMU 'B' T/M	"	60		X	4.99K $\Omega$	AC
BODY RATE, COM. 'B' $\omega$ xc HI, DMU 'B' T/M	"	61		X	4.99K $\Omega$	AC
GYRO #2 TEMP. DMU 'B' T/M	"	62		X	4.99K $\Omega$	AC
GYRO #4 TEMP. DMU 'B' T/M	"	63		X	4.99K $\Omega$	AC
GYRO #6 TEMP. DMU 'B' T/M	"	64		X	4.99K $\Omega$	AC
GYRO #2 $\phi$ B MOTOR CURRENT, DMU 'B' T/M	"	65		X	4.99K $\Omega$	AC
GYRO #4 $\phi$ B MOTOR CURRENT, DMU 'B' T/M	"	66		X	4.99K $\Omega$	AC
GYRO #6 $\phi$ B MOTOR CURRENT, DMU 'B' T/M	"	67		X	4.99K $\Omega$	AC
GYRO #2 RATE HI. DMU 'B' T/M	"	68		X	4.99K $\Omega$	AC
GYRO #4 RATE HI. DMU 'B' T/M	"	69		X	4.99K $\Omega$	AC
GYRO #6 RATE HI. DMU 'B' T/M	"	70		X	4.99K $\Omega$	AC
SPARE	"	71				
SPARE	"	72				
SPARE	"	73				
SPARE	"	74				
SPARE	"	75				
SPARE	"	76				
SPARE	"	77				
SHIELD	"	78				

[illegible]

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DETAILED ELECTRICAL  
(CONTINUED)

FUNCTION	CONNECTOR	PIN#	INPUT	OUTPUT	Z <sub>S</sub> or Z <sub>L</sub>	CKT
+15 VDC, GYRO #1	TEST (J2)	1		X	100K $\Omega$	
+10 VDC, GYRO #1	"	2		X	100K $\Omega$	
-10 VDC, GYRO #1	"	3		X	100K $\Omega$	
+ 5 VDC, GYRO #1	"	4		X	100K $\Omega$	
+15 VDC, GYRO #2	"	5		X	100K $\Omega$	
+10 VDC, GYRO #2	"	6		X	100K $\Omega$	
-10 VDC, GYRO #2	"	7		X	100K $\Omega$	
+ 5 VDC, GYRO #2	"	8		X	100K $\Omega$	
+15 VDC, GYRO #3	"	9		X	100K $\Omega$	
+10 VDC, GYRO #3	"	10		X	100K $\Omega$	
-10 VDC, GYRO #3	"	11		X	100K $\Omega$	
+ 5 VDC, GYRO #3	"	12		X	100K $\Omega$	
+15 VDC, GYRO #4	"	13		X	100K $\Omega$	
+10 VDC, GYRO #4	"	14		X	100K $\Omega$	
-10 VDC, GYRO #4	"	15		X	100K $\Omega$	
+ 5 VDC, GYRO #4	"	16		X	100K $\Omega$	
+15 VDC, GYRO #5	"	17		X	100K $\Omega$	
+10 VDC, GYRO #5	"	18		X	100K $\Omega$	
-10 VDC, GYRO #5	"	19		X	100K $\Omega$	
+ 5 VDC, GYRO #5	"	20		X	100K $\Omega$	
+15 VDC, GYRO #6	"	21		X	100K $\Omega$	
+10 VDC, GYRO #6	"	22		X	100K $\Omega$	
-10 VDC, GYRO #6	"	23		X	100K $\Omega$	
+ 5 VDC, GYRO #6	"	24		X	100K $\Omega$	
SIM. TORQUING COMMAND	"	25	X			DI
SIM. TORQ. SIG. GYRO #1	"	26	X		4.7K $\Omega$	
SIM. TORQ. SIG. GYRO #2	"	27	X		4.7K $\Omega$	
SIM. TORQ. SIG. GYRO #3	"	28	X		4.7K $\Omega$	
SIM. TORQ. SIG. GYRO #4	"	29	X		4.7K $\Omega$	
SIM. TORQ. SIG. GYRO #5	"	30	X		4.7K $\Omega$	
SIM. TORQ. SIG. GYRO #6	"	31	X		4.7K $\Omega$	
MICROSYN EXC. GYRO #1 HI	"	32		X	10 K $\Omega$	
MICROSYN EXC. GYRO #2 HI	"	33		X	10 K $\Omega$	
MICROSYN EXC. GYRO #3 HI	"	34		X	10K $\Omega$	
MICROSYN EXC. GYRO #4 HI	"	35		X	10K $\Omega$	
MICROSYN EXC. GYRO #5 HI	"	36		X	10K $\Omega$	
MICROSYN EXC. GYRO #6 HI	"	37		X	10K $\Omega$	

FOLDOUT FRAME



OUTPUT	Z <sub>S</sub> or Z <sub>L</sub>	CKT. TYPE	VOLT. RANGE	REMARKS
X	100K Ω		VALUE ± 5%	100K Ω IN SERIES WITH SUPPLY
X	100K Ω		"	"
X	100K Ω		"	"
X	100K Ω		"	"
X	100K Ω		"	"
X	100K Ω		"	"
X	100K Ω		"	"
X	100K Ω		"	"
X	100K Ω		"	"
X	100K Ω		"	"
X	100K Ω		"	"
X	100K Ω		"	"
X	100K Ω		"	"
X	100K Ω		"	"
X	100K Ω		"	"
X	100K Ω		"	"
X	100K Ω		"	"
X	100K Ω		"	"
X	100K Ω		"	"
X	100K Ω		"	"
X	100K Ω		"	"
X	100K Ω		"	"
X	100K Ω		"	"
X	100K Ω		"	"
X	100K Ω		"	"
		DJ-4		REQUIRES GROUNDING TO ACTIVATE COMMAND
	4.7K Ω		± 5 VDC	
	4.7K Ω		± 5 VDC	
	4.7K Ω		"	
	4.7K Ω		"	
	4.7K Ω		"	
	4.7K Ω		"	
X	10 K Ω		2VRMS ± 2%	9.6 KHZ
X	10 K Ω		"	"
X	10K Ω		"	"
X	10K Ω		"	"
X	10K Ω		"	"
X	10K Ω		"	"

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DETAILED ELECTRICAL  
(CONTINUED)

FUNCTION	CONNECTOR	PIN#	INPUT	OUTPUT	Z <sub>S</sub> or Z <sub>L</sub>	CK
GYRO #1 HTR DUTY CYCLE HI	"	44		X	100K $\Omega$	
GYRO #2 HTR DUTY CYCLE HI	"	45		X	100K $\Omega$	
GYRO #3 HTR DUTY CYCLE HI	"	46		X	100K $\Omega$	
GYRO #4 HTR DUTY CYCLE HI	"	47		X	100K $\Omega$	
GYRO #5 HTR DUTY CYCLE HI	"	48		X	100K $\Omega$	
GYRO #6 HTR DUTY CYCLE HI	"	49		X	100K $\Omega$	
HTR DUTY CYCLE GND	"	50				
4V SUSP. COMMAND	"	51	X			D
FF COMMAND	"	52	X			D
SPARE	"	53				
SPARE	"	54				
SPARE	"	55				
GYRO #1 WHEEL VOLTS $\phi$ A HI	"	56		X	10K $\Omega$	
GYRO #1 WHEEL VOLTS $\phi$ A LO	"	57		X	10K $\Omega$	
GYRO #2 WHEEL VOLTS $\phi$ A HI	"	58		X	10K $\Omega$	
GYRO #2 WHEEL VOLTS $\phi$ A LO	"	59		X	10K $\Omega$	
GYRO #3 WHEEL VOLTS $\phi$ A HI	"	60		X	10K $\Omega$	
GYRO #3 WHEEL VOLTS $\phi$ A LO	"	61		X	10K $\Omega$	
GYRO #4 WHEEL VOLTS $\phi$ A HI	"	62		X	10K $\Omega$	
GYRO #4 WHEEL VOLTS $\phi$ A LO	"	63		X	10K $\Omega$	
GYRO #5 WHEEL VOLTS $\phi$ A HI	"	64		X	10K $\Omega$	
GYRO #5 WHEEL VOLTS $\phi$ A LO	"	65		X	10K $\Omega$	
GYRO #6 WHEEL VOLTS $\phi$ A HI	"	66		X	10K $\Omega$	
GYRO #6 WHEEL VOLTS $\phi$ A LO	"	67		X	10K $\Omega$	
WHEELS DISABLE	"	68	X			I
SUSP. EXC. GYRO #1 HI	"	69		X	1K	
SUSP. EXC. GYRO #2 HI	"	70		X	1K	
SUSP. EXC. GYRO #3 HI	"	71		X	1K	
SUSP. EXC. GYRO #4 HI	"	72		X	1K	
SUSP. EXC. GYRO #5 HI	"	73		X	1K	
SUSP. EXC. GYRO #6 HI	"	74		X	1K	
SUSP. CURR. GYRO #1 TG LO	"	75		X	1K	
SUSP. CURR. GYRO #1 SG LO	"	76		X	1K	

FOLDOUT FRAME

DETAILED ELECTRICAL INTERFACE  
(CONTINUED)

PUT	OUTPUT	$Z_S$ or $Z_L$	CKT. TYPE	VOLT. RANGE	REMARKS
	X	100K $\Omega$		28VDC OR 0 VDC	600 Hz PWM WAVEFORM
	X	100K $\Omega$		"	"
	X	100K $\Omega$		"	"
	X	100K $\Omega$		"	"
	X	100K $\Omega$		"	"
	X	100K $\Omega$		"	"
X			DI-4		REQUIRE GROUNDING TO ACTIVATE COMMAND
X			DI-4		REQUIRE GROUNDING TO ACTIVATE COMMAND
	X	10K $\Omega$		34VRMS OR 18VRMS	$\pm 5\%$ ON VOLTAGE, 960 Hz
	X	10K $\Omega$			
	X	10K $\Omega$		34VRMS OR 18VRMS	$\pm 5\%$ ON VOLTAGE, 960 Hz
	X	10K $\Omega$			
	X	10K $\Omega$		34VRMS OR 18VRMS	$\pm 5\%$ ON VOLTAGE, 960 Hz
	X	10K $\Omega$			
	X	10K $\Omega$		34VRMS OR 18VRMS	$\pm 5\%$ ON VOLTAGE, 960 Hz
	X	10K $\Omega$			
	X	10K $\Omega$		34VRMS OR 18VRMS	$\pm 5\%$ ON VOLTAGE, 960 Hz
	X	10K $\Omega$			
X			DI-4		REQUIRE GROUNDING TO ACTIVATE COMMAND
	X	1K		2.5 OR 4 VRMS	$\pm 2\%$ ON VOLTAGE, 9.6 KHz
	X	1K		"	"
	X	1K		"	"
	X	1K		"	"
	X	1K		"	"
	X	1K		"	"
	X	1K		50 MV RANGE	1 $\Omega$ RESISTOR
	X	1K		"	"

FOLDOUT FRAME 2

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[illegible]

FOLDOUT FRAME



[illegible]

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## 12.0 APPENDIX A

IUE FLIGHT SYSTEM

TEST DATA SUMMARY

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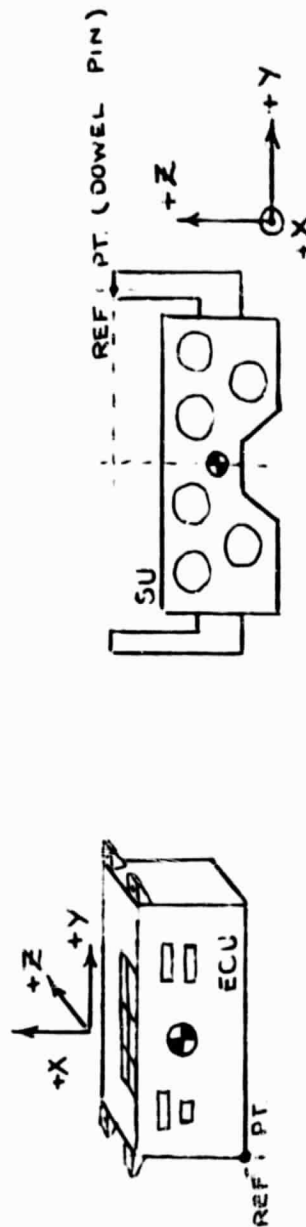
PHYSICAL MEASUREMENT, WEIGHT, POWER, CG

PHYSICAL MEASUREMENTS - MEETS OUTLINE DIMENSIONS

WEIGHT = 48.35 LBS. (21.9KG) SPEC = 39.02 LBS. (17.7KG)

POWER = 74.2 WATTS (IN THERMAL VACUUM) SPEC = 67 WATTS

CENTER OF GRAVITY - CG COORDINATES FROM REFERENCE POINT (CM)



	X	Y	Z
ECU	+2.037	-23.749	-15.194
SU	+0.802	- 9.35	- 5.982

BANDWIDTH MEASUREMENTS

RS#	THROUGH MATRIX OUTPUTS (HZ)				THROUGH BUFFERED RATE OUTPUT HOLD-SLEW AT 135°F
	RATE COLD 80°F	RATE NORMAL 110°F	RATE NORMAL 135°F		
1	2.4	1.4	6.4	8.1	
2	2.7	1.6	6.1	7.3	
3	2.8	1.6	6.2	9.0	
4	2.8	2.0	6.6	10.1	
5	2.7	1.7	7.1	9.4	
6	3.4	2.0	6.9	10.3	
SPEC LIMITS	1.4 HZ	1.4 HZ	4.0 HZ	5.0 HZ	



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BIAS DRIFT (G AND NON-G SENSITIVE)

	G1	G2	G3	G4	G5	G6	SPEC.
<u>INITIAL PERE</u>							
MUSA	+1.325	+ .655	+ .131	- .194	+ .809	- .543	10 <sup>0</sup> /HR/G
MUTA	-2.349	- .443	.210	- .107	.533	.166	10 <sup>0</sup> /HR/G
NON-G SENS	- .032	+ .752	+ .617	- .222	- .926	- .974	5 <sup>0</sup> /HR
<u>FINAL PERE</u>							
MUSA	1.041	.883	.132	- .158	.793	- .657	10
MUTA	-1.801	- .734	.064	- .084	.578	.007	10
NON-G SENS	+ .006	+ .753	+ .625	- .238	- .925	- .965	5
<u>STABILITY</u>							
MUSA	.284	.234	.001	.036	.016	.114	1
MUTA	.548	.291	.146	.023	.045	.173	1
NON-G SENS	.038	.001	.008	.016	.001	.009	0.5

ALIGNMENT DELTAS FROM IDEAL - X AXIS

	G <sub>1</sub>	G <sub>2</sub>	G <sub>3</sub>	G <sub>4</sub>	G <sub>5</sub>	G <sub>6</sub>	SPEC
INITIAL PERF.	-33	14	-211	25	51	64	+240 ARC SEC
FINAL PERF.	-22	25	-200	10	42	66	+240 ARC SEC
STABILITY	5.5	5.5	5.5	7.5	4.5	1.0	+15 ARC SEC

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ALIGNMENT DELTAS FROM IDEAL - Y AXIS

	G <sub>1</sub>	G <sub>2</sub>	G <sub>3</sub>	G <sub>4</sub>	G <sub>5</sub>	G <sub>6</sub>	SPEC
INITIAL PERF.	-111	-7	31	-65	107	-80	+240 ARC SEC
FINAL PERF.	-118	-5	23	-22	104	-52	+240 ARC SEC
STABILITY	3.5	1.0	4.0	21.5	1.5	11.0	+15 ARC SEC

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ALIGNMENT DELTAS FROM IDEAL - Z AXIS

	G <sub>1</sub>	G <sub>2</sub>	G <sub>3</sub>	G <sub>4</sub>	G <sub>5</sub>	G <sub>6</sub>	SPEC
INITIAL PERF.	55	-90	53	-2	184	-57	+240 ARC SEC
FINAL PERF.	100	-20	22	-43	103	-40	+240 ARC SEC
STABILITY	22.5	35	16.5	20.5	40.5	8.5	+15 ARC SEC

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MEAN SCALE FACTORS (DIGITAL) - 3 OCCURRENCES

	G <sub>1</sub>	G <sub>2</sub>	G <sub>3</sub>	G <sub>4</sub>	G <sub>5</sub>	G <sub>6</sub>	SPEC.
H/S MODE	.0101085213	.0100343033	.0100298682	.0100334612	.0101326036	.0100453515	0.01 TO 0.10
RATE MODE	.31376335	.31009669	.311684286	.30861975	.31329002	.311866792	NO REQ'T

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SCALE FACTOR LINEARITY - BIAS METHOD LAST OCCURRENCE

INPUT RATE (°/HR)	G1	G2	G3	G4	G5	G6
+50	-27	91	194	86	-29	-3
-50	+94	103	-127	-54	140	91
+100	-86	32	-98	12	-71	-76
-100	63	-4	103	-23	59	133
+200	-52	-77	-59	48	-44	-106
-200	11	12	19	-34	31	+61
+300	-49	-73	-52	20	-38	-8
-300	20	4	8	-22	4	-46
+400	-25	-66	-18	51	-14	34
-400	25	21	22	-26	-6	-36
+600	-22	-83	-3	13	-30	-11
-600	49	41	11	-71	-4	-33
LIMIT (PPM)	1000	1000	1000	1000	1000	1000

SCALE FACTOR STABILITY (50 DAYS) - WORST CASE

	G <sub>1</sub>	G <sub>2</sub>	G <sub>3</sub>	G <sub>4</sub>	G <sub>5</sub>	G <sub>6</sub>
+50°/HR	-21	-46	-43	-23	-183	103
+100°/HR	-30	39	-65	16	-144	-104
+200°/HR	-31	-18	-65	-16	-135	-91
+300°/HR	-29	-43	-62	-12	-88	-83
+400°/HR	-29	-48	-66	12	-71	-91
+600°/HR	-38	-42	-66	32	-37	-76
$\bar{M}$	29.6	26.3	61.1	1.5	109.6	57.0

SPEC LIMIT = 100 PPM/35 DAYS

COMPUTE  
AVERAGES

BIAS DRIFT STABILITY RESULTS

	G <sub>1</sub>	G <sub>2</sub>	G <sub>3</sub>	G <sub>4</sub>	G <sub>5</sub>	G <sub>6</sub>	SPEC
<u>INITIAL PERF.</u>							
RATE RAMP	-0.00007	-0.00002	0.000007	-0.00011	-0.00002	0.00002	0.0004 o/HR/HR
SHORT TERM	0.00123	0.00327	-0.00171	0.00178	-0.00369	0.00237	0.005 o/HR
<u>FINAL PERF.</u>							
RATE RAMP	-0.00006	-0.00013	-0.00004	0.00005	0.00006	0.00008	0.0004
SHORT TERM	0.0011	0.0031	0.0020	0.0019	0.0040	0.0030	0.005



SHORT TERM ATTITUDE NOISE RESULTS

	RS #1	RS #2	RS #3	RS #4	RS #5	RS #6	SPEC.
5 MIN. ABS.	-0.09	-0.09	-0.11	-0.27	-0.04	0.08	1 ARC SEC
30 MIN. ABS.	-0.30	-0.04	0.39	-0.66	-0.25	-0.10	2 ARC SEC
RMS - 5 MIN.	0.06	0.05	0.06	0.07	0.05	0.06	0.33
30 MIN.	0.06	0.05	0.06	0.07	0.05	0.06	0.67
POINT/POINT MAX.	.21	0.20	.20	.20	0.20	0.20	0.20
5 MIN. ABS.	0.26	0.14	-0.12	-0.06	-0.07	-0.23	1 ARC SEC.
30 MIN. ABS.	0.38	0.71	0.03	-0.26	-0.90	-0.87	2 ARC SEC.
RMS - 5 MIN.	0.08	0.06	0.07	0.08	0.06	0.07	0.33
30 MIN.	0.07	0.06	0.07	0.07	0.05	0.07	0.67
POINT/POINT MAX.	0.20	0.20	0.21	0.20	0.20	0.21	0.20

MATRIX OUTPUTS - SCALE FACTOR

MODE	AXIS	MATRIX "A"	MATRIX "B"	SPEC
RATE COLD	X	0.962	0.959	$1+.075V/^{\circ}/SEC$
	Y	0.957	0.961	
	Z	0.959	0.958	
RATE NORMAL	X	0.965	0.958	$1+.075V/^{\circ}/sec$
	Y	0.958	0.958	
	Z	0.957	0.958	
HOLD/ SLEW	X	0.049	0.049	$0.050+.00375$ $V/ARC SEC/SEC$
	Y	0.049	0.049	
	Z	0.0496	0.0495	

BIAS COMPENSATION

	AXIS	SPEC (H/S)	ACTUAL	
			MATRIX "A"	MATRIX "B"
RANGE (SEC/SEC)	X Y Z	NO REQUIREMENT	+ 306 - + 25.5 - + 25.5 -	+ 306 - + 25.5 - + 25.5 -
SCALE FACTOR (MATRIX OUTPUT) MV <sup>0</sup> /HR	X Y Z	600 ± 45 50 ± 3.75 50 ± 3.75	595.2 49.98 50.01	595.2 49.69 49.97
RESOLUTION (SEC/BIT)	X Y Z	0.60 0.05 0.05	0.60 0.05 0.05	0.60 0.05 0.05

## BODY RATE OUTPUTS - RIPPLE, NOISE, NONLINEARITIES

RATE COLD		DEVIATION FROM MEAN (VDC)			
AXIS	RATE( <sup>o</sup> /S)	MATRIX A	MATRIX B	LIMITS (VDC)	
X	+1.0	.021	.001	A	.080
	-1.0	.019	.001		
	+2.5	.032	.001	B	.080
	-2.5	.025	.002		
	+5.0	.011	.006	(300 SEC/SEC)	
	-5.0	.037	.001		
Y	+1.0	.002	.001	A	.019
	-1.0	.003	0		
	+2.5	.004	.001	B	.019
	-2.5	.004	.001		
	+5.0	.007	.002	(72 SEC/SEC)	
	-5.0	.001	.003		
Z	+1.0	.002	.001	A	.019
	-1.0	.003	.001		
	+2.5	.003	0	B	.019
	-2.5	.002	.002		
	+5.0	.007	0	(72 SEC/SEC)	
	-5.0	.001	.004		

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## BODY RATE OUTPUTS - RIPPLE, NOISE, NONLINEARITIES

RATE NORMAL		DEVIATION FROM MEAN (VDC)			
AXIS	RATE( <sup>o</sup> /SEC)	MATRIX A	MATRIX B	LIMITS (VDC)	
X	+1.0	.020	.003	A	.064
	-1.0	.001	.006		
	+2.5	.003	.007	B	.064
	-2.5	.016	.005		
	+5.0	.035	.017	(240 SEC/SEC)	
	-5.0	.030	.006		
	y	+1.0	.001	.002	A
-1.0		.001	.001		
+2.5		.002	.001	B	.0106
-2.5		.003	.002		
+5.0		.005	.001	(40 SEC/SEC)	
-5.0		.001	.003		
Z		+1.0	.003	.001	A
	-1.0	.001	.002		
	+2.5	.003	0	B	.0106
	-2.5	.003	0		
	+5.0	0	.002	(40 SEC/SEC)	
	-5.0	.002	.001		

## BODY RATE OUTPUTS - RIPPLE, NOISE, NONLINEARITIES

HOLD/SLEW		DEVIATION FROM MEAN (VDC)			
AXIS	RATE (SEC/SEC)	MATRIX A	MATRIX B	LIMITS (VDC)	
X	+25.0	.044	.012	A	.392
	-25.0	.009	.018	B	.394
	+50.0	.108	.024		
	-50.0	.001	.016	(8.0 SEC/SEC)	
	+100.0	.294	.012		
	-100.0	.139	.018		
	Y	+25.0	.006	.002	A
-25.0		.019	.003	B	.0344
+50.0		.018	.008		
-50.0		.012	.005	(0.7 SEC/SEC)	
+100.0		.032	.013		
-100.0		.005	.011		
Z		+25.0	.030	.001	A
	-25.0	.012	.001		
	+50.0	.010	.010	B	.0346
	-50.0	.030	.004		
	+100.0	.013	.007	(0.7 SEC/SEC)	
	-100.0	.028	.020		

MATRIX NULLS -  $X_{UP}$ ,  $Y_{WEST}$ ,  $Z_{SOUTH}$ 

AXIS	MATRIX A	MATRIX B	STATE
X	-15 MV	+17 MV	RATE COLD (80°F) G-TEMP <1.5 VDC
Y	+3 MV	-3 MV	
Z	-2.5 MV	+1 MV	
X	-8 MV	+39 MV	RATE NORMAL (110°F) G-TEMP <2.4 VDC)
Y	+4.4 MV	-4.5 MV	
Z	-2.6 MV	-1.4 MV	
X	-16 MV	+44 MV	RATE NORMAL (135°F) G-TEMP STABILIZED
Y	+5 MV	-3 MV	
Z	-3 MV	-1.5 MV	
X	+290 MV	+620 MV	HOLD/SLEW (135°F) G-TEMP STABILIZED
Y	-12 MV	-63 MV	
Z	-522 MV	-516 MV	